## VOLUMETRIC SURVEY OF WELSH RESERVOIR

## Prepared for: <br> AEP/Southwestern Electric Power Company

In cooperation with the Northeast Texas Municipal Water District


Prepared by<br>Texas Water Development Board

# Texas Water Development Board 

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Published and Distributed by the

Texas Water Development Board
P.O. Box 13231

Austin, Texas 78711-3231

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# WELSH RESERVOIR VOLUMETRIC SURVEY REPORT 

## INTRODUCTION


#### Abstract

Staff of the Surface Water Section of the Texas Water Development Board (TWDB) conducted a volumetric survey of Welsh Reservoir on November 27 and 28, 2001. The primary purpose of this survey was to determine the current volume of the reservoir at conservation pool elevation. Results from this survey will serve as a basis for comparison to future surveys to allow the location and rates of sediment deposition to be determined. Survey results are presented in the following pages in both graphical and tabular form.


The vertical datum used during this survey is based on the reservoir gauge that is maintained by the American Electric Power/Southwestern Electric Power Company who operates the reservoir and electric power-generating plant. The datum for this gauge is reported at mean sea level (msl). Thus, elevations are reported here in feet ( ft ) above mean sea level (msl). Volume and area calculations in this report are referenced to water levels provided by the reservoir gauge.

According to the original design information, the surface area was 1,365 acres at conservation pool elevation 320.0 ft ; the total storage volume was estimated to be 23,587 acre-feet (ac-ft) of water (Camp Dresser \& McKee Consulting Engineers, Phase I Inspection Report National Dam Safety Program, 1979). This report will compare the 2001 survey results with the original design information developed in 1974.

## RESERVOIR HISTORY AND GENERAL INFORMATION

Welsh Reservoir and associated Welsh Dam (formerly Swauano Creek Dam) is located on Swauano Creek (Cypress River Basin) in Titus County, approximately 12 miles southeast of Mt. Pleasant, Texas (Figure 1). At conservation pool elevation (320.0 ft ), the reservoir extends approximately 5 miles upstream on Swauano Creek. Records indicate the drainage area is approximately 21.75 square miles. At conservation pool elevation the reservoir has approximately 25 miles of shoreline. Welsh Reservoir and Dam were designed for industrial and recreational use.

American Electric Power /Southwestern Electric Power Company (AEP/SWEPCO) owns the water rights to Welsh Reservoir. AEP/SWEPCO also owns and maintains the dam and appurtenant structures. All releases from the reservoir and other water-related operations are under the control of AEP/SWEPCO.

The Texas Water Rights Commission granted Water Rights Permit No. 2926 (Application No. 3164) to Southwestern Electric Power Company (SWEPCO) on May 30, 1974. The permit allowed SWEPCO "to construct a dam and reservoir on Swauano Creek in Titus County and impound therein not to exceed 23,587 ac-ft of water." SWEPCO was authorized to divert, circulate and recirculate, and to consumptively use not to exceed 11,000 ac-ft from the reservoir. The right to use the impounded waters for recreation purposes was also granted.

AEP/SWEPCO's current authorization is based on Certificate of Adjudication \# 04-4576 issued by the Texas Water Commission on October 13, 1986. The certificate authorizes SWEPCO to maintain an existing dam and reservoir (Welsh Reservoir) on Swauano Creek and impound therein not to exceed $23,587 \mathrm{ac}-\mathrm{ft}$ of water.

The owner of the certificate is authorized to divert, ciculate, recirculate and use consumptively not to exceed $11,000 \mathrm{ac}-\mathrm{ft}$ of water per annum for industrial purposes.

The owner is also authorized to use the impounded water in the reservoir for recreational purposes.

Copies of the Permits and Certificate of Adjudication (original and amended) may be obtained from the Texas Natural Resource Conservation Commission's Central Records in Austin, Texas.

Construction for the Welsh Reservoir Project started June 24,1974 and was completed September 25,1975. Deliberate impoundment of water began September 29,1975 (Freese and Nichols Inc. Consulting Engineers, Safety Inspection of Swauano Creek Dam at Welsh Power Plant, September 1989). Freese and Nichols Inc. Consulting Engineers was the design engineer and the construction contractor was List \& Clark Construction Company of Overland Park, Kansas (Camp, Dresser \& McKee, Inc., 1979).

Engineering designs (Camp, Dresser \& McKee, Inc., 1979) show Welsh Dam and appurtenant structures to consist of an earth fill embankment, approximately $4,800 \mathrm{ft}$ in length with a maximum height of 60 ft and a crest elevation of 335.0 ft . The upstream slope of the embankment is protected by a soil-cement for erosion control.

The service spillway is an uncontrolled reinforced concrete morning glory structure and is located near the left (east) end of the embankment. Discharges pass through the embankment downstream via a 7 - ft wide by 8 - ft tall box conduit. The crest elevation of the morning glory is 320.0 ft .

The emergency spillway is a $1,500-\mathrm{ft}$ wide trapezoidal shape earth cut channel located at the right (west) end of the embankment. The crest elevation of the emergency spillway is 326.0 ft .

The outlet works or regulating outlet consists of an 18-inch pipe connected to the service spillway discharge conduit. The invert elevation of the 18 -inch pipe is 295.0 ft . Dual valves control releases.

## SURVEYING EQUIPMENT

The equipment used to perform the volumetric survey consists of a 20 -foot aluminum shallow-draft flat bottom SeaArk craft with cabin and equipped with one 115horsepower Evinrude outboard motor. The portable data collection equipment on-board the boat included a Knudsen $320 \mathrm{~B} / \mathrm{P}$ Echosounder (depth sounder), a Trimble Navigation, Inc. Ag132 GPS receiver with OmniSTAR (for differential corrections) and a laptop PC.

The GPS equipment, survey vessel, and depth sounder in combination provide an efficient hydrographic survey system. As the boat travels across the reservoir's surface, the depth sounder takes approximately ten readings of the reservoir's bottom each second. The depth readings are stored on the survey vessel's on-board computer along with the corrected positional data generated by the boat's GPS receiver. The data files collected are downloaded from the computer and brought to the office for editing after the survey is completed. During editing, poor-quality data is removed or corrected, multiple data points are averaged to get one data point per second, and average depths are converted to elevation readings based on the reservoir's elevation, recorded on the day the survey was performed. Accurate estimates of the reservoir's volume can be determined by building a 3-D model of the reservoir from the collected data.

## PRE-SURVEY PROCEDURES

The reservoir's boundary was digitized using Environmental Systems Research Institute's (ESRI) Arcview from digital orthophoto quadrangle images (DOQ's). The DOQ's were produced by VARGIS of Texas LLC for the TEXAS Orthoimagery Program (TOP). The DOQ products produced for the Department of Information Resources and the GIS Planning Council under the Texas Orthoimagery Program reside in the public domain. More information can be obtained on the Internet at http://www.tnris.state.tx.us/DigitalData/doqs.htm. The map boundary was created from
the CASON, TEXAS DOQs and Digital Raster Graphics (DRG's) which are digital versions of 7.5 -minute topographical maps. The reservoir's elevation at the time the DOQs were photographed was 320.17 ft on March 09,1995 and 317.20 on January 6, 1996. The DRG was photo-revised in 1980. The boundary was completed by overlaying the survey data points and comparing to the above digital maps making sure that all survey data were within the boundary and using the DRG to compensate for the low water level in the January 6, 1996 photo.

The DOQ and DRG graphic boundary files were transformed from UTM Zone 14 datum to NAD ‘83, using Environmental Systems Research Institute’s (ESRI) Arc/Info PROJECT command with the NADCOM (standard conversion method within the United States) parameters.

The survey layout was designed by placing survey track lines at 500 -foot intervals within the digitized reservoir's boundary using Coastal Oceanographics' HYPACK software. The survey design required the use of approximately 90 survey lines along the length of the reservoir and perpendicular to the original creek channels.

## SURVEY PROCEDURES

## Equipment Calibration and Operation

At the beginning of each day of the survey, the depth sounder is calibrated using the bar check feature in the Knudsen software program. This is accomplished by positioning the transducer over a known (measured) depth. The value for the speed of sound is adjusted in the software (either higher or lower) until the displayed depths matched the known depth. The depth is then checked manually with a stadia (survey) rod to ensure that the depth sounder is properly calibrated and operating correctly.

While surveying Welsh Reservoir, the speed of sound in the water column was 4,750 feet per second. Based on the measured speed of sound for various depths and the average speed of sound calculated for the entire water column, the depth sounder is accurate to within $\pm 0.2$ feet. An additional estimated error of $\pm 0.3$ feet arises from variation in boat inclination. These two factors combine to give an overall accuracy of $\pm 0.5$ feet for any instantaneous reading. These errors tend to be minimized over the entire survey, since some readings are positive and some are negative. Further information on these calculations is presented in Appendix G.

During the survey, the horizontal mask setting on the on-board GPS receiver was set to 10 degrees and the PDOP (Position Dilution of Precision) limit was set to 7 to maximize the accuracy of the horizontal positioning. An internal alarm sounds if PDOP rises above seven to advise the field crew that the horizontal position has degraded to an unacceptable level. The lake's initialization file used by the HYPACK data collection program was set up to convert the collected DGPS positions to state-plane coordinates on the fly.

## Field Survey

TWDB staff collected data at Welsh Reservoir on November 27 and 28, 2001. The lake-level elevation remained constant at 319.9 ft . The weather and surface water conditions were excellent for the first day of data collection. A northern cold front blew in early on the second day of the survey. Strong thunderstorms and high winds delayed the data collection for approximately four hours. The survey crew was able to complete the survey later that afternoon.

The survey crew began at the dam and collected data on pre-plotted range lines (transects) that were spaced 500 feet apart and designed to be perpendicular to the channel for the best cross-section results. A data point that consisted of latitude, longitude and depth was collected each second. Data were collected on 87 of the 90 preplotted survey range lines. The survey crew also collected data on irregular transects
when navigational hazards such as trees and stumps or shallow depths kept the crew from driving on the pre-plotted lines. Approximately 22056 data points were collected over the 36.2 miles traveled during the survey. These points, shown in Figure 2, were stored digitally on the boat's computer in 120 data files.

The topography at Welsh Reservoir was typical of the East Texas Rolling Hills Region with elevated terrain occupied by mostly pine trees. The catchment basin of Welsh Reservoir is located on Swauano Creek and lies in a north to south direction with Welsh Dam located at the south end of the reservoir. There are several small tributaries (unnamed) that empty into the main basin from the east and west sides of the reservoir.

Welsh Electric-generating Power Plant is located along the west bank of the main catchment basin of Welsh Reservoir. Water is circulated throughout the reservoir for cooling purposes for the power plant. The intake channel is located on the west bank near the dam. Water is pumped through the power plant and is discharged upstream of the power plant and catchment basin. This allows the water to cool in the main body of the reservoir before being recirculated through the power plant. The survey crew was unable to collect data in all portions of the intake and discharge channels because of security structures. Due to the volume of water flowing through these channels, it is expected there is a minimum amount of sediment located in the channels.

Mr. Winston Holley of American Electric Power provided an estimate of the surface area and volume of the discharge pocket and canal that were not accessible by TWDB staff during their survey. The area given was 60 surface acres with an estimated average depth of 10 ft . Assuming a retangular profile the resulting $600 \mathrm{ac}-\mathrm{ft}$ of volume was evenly distributed over the upper ten feet of the reservoir and are included in Appendix A (Reservoir Volume Table). The Digitial Terrain Model described in the following section uses the input boundary file including the discharge pocket and canal as the final area at conservation pool elevation.

Only a few residences were noted along the east bank in the main basin. A public boat ramp was located on the west bank in the upper end of the reservoir. The remainder
of the land surrounding the lake was left undisturbed. The fact that a limited amount of development was present or the lack of fishing piers and boat ramps on Welsh Reservoir made it easier for the survey crew to collect data along the shoreline.

Native plants and ground cover was observed around the majority of the reservoir's shoreline. No major shoreline erosion was observed.

As data were collected along the pre-plotted transects, the survey crew noticed that the lake bottom was generally flat. At times there was evidence of the original creek channel (thalweg) when the survey crew crossed over Swauano Creek.

The majority of the lake was clear of navigational hazards such as trees, rocks and debris. It was only in the upper reaches of the lake and in the channel of the Swauano Creek that the crew encountered such hazards.

## Data Processing

The collected data were downloaded from diskettes onto TWDB's network disk drives. Tape backups were made for future reference. To process the data, the EDIT routine in the HYPACK Program was run on each raw data file. Data points such as depth spikes or data with missing depth or positional information were deleted from each file. A correction for the reservoir elevation at the time of data collection was also applied to each file during the EDIT routine. During the November survey, the water surface remained at elevation 319.9 ft according to elevation data provided by the AEP/SWEPCO gauge. After all corrections were applied to the raw data file, the edited file was saved with a different extension. The edited files were combined into a single ( $\mathrm{x}, \mathrm{y}, \mathrm{z}$ ) data file which was used with the GIS software to develop a model of the lake's bottom surface.

The resulting data file was downloaded to a Dell Precision 410 workstation running the Microsoft's Windows NT 4.0 with service pack 6.0, Environmental System

Research Institute's (ESRI) ArcGIS software was used to convert the data to a MASS points file. The MASS points and the boundary file were then used to create a Digital Terrain Model (DTM) of the lake's bottom surface using Arc/Info's TIN software module. The module generates a triangulated irregular network (TIN) from the data points and the boundary file using a method known as Delauney's criteria for triangulation. A triangle is formed between three non-uniformly spaced points, including all points along the boundary. If there is another point within the triangle, additional triangles are created until all points lie on the vertex of a triangle. All of the data points are used in this method. The generated network of three-dimensional triangular planes represents the actual bottom surface. With this representation of the bottom, the software then calculates elevations of each triangular surface plane by determining the elevation along the leg of each triangle. The reservoir area and volume can be determined from the triangulated irregular network created using this method of interpolation. Volumes and area were calculated from the TIN for the entire reservoir at one-tenth of a foot interval from minimum elevation to conservation pool level. From elevation $276.1-\mathrm{ft}$ to $320-\mathrm{ft}$, the surface areas and volumes of the reservoir were computed using the ArcGIS software. The computed reservoir volume table is presented in Appendix A and the area table is presented in Appendix B. Graphs for the volume and area tables can be found in Appendix C and D respectively.

Other products developed from the model include a shaded elevation range map (Figure 3) and a shaded depth range map (Figure 4). To develop these maps, the TIN was converted to a lattice using the TINLATTICE command and then to a polygon coverage using the LATTICEPOLY command. Linear filtration algorithms were applied to the DTM to produce smooth cartographic contours. The resulting elevation contour map of the bottom surface at two-foot intervals is presented in Figure 5.

## RESULTS

Results from the 2001 TWDB survey indicate Welsh Reservoir encompasses 1,269 surface acres and contains a total volume of 20,242 ac-ft at the conservation pool
elevation of 320.0 ft msl (gauge datum). Dead pool storage, the volume below the invert elevation of the low-flow outlet pipe at 295.0 ft is 1811 ac- ft . Thus, the usable conservation storage (total volume - dead storage) for Welsh Reservoir is $18,431 \mathrm{ac}-\mathrm{ft}$. The shoreline at conservation pool elevation was calculated to be approximately 25 miles. The deepest point that was measured during the survey was at elevation 276.1 ft and corresponding to a depth of 43.9 ft was located approximately 600 ft upstream from Welsh Dam.

## SUMMARY AND COMPARISONS

Welsh Reservoir was completed in September 1975. Storage calculations in 1974 (Camp Dresser \& McKee Consulting Engineers, Phase I Inspection Report National Dam Safety Program, 1979) reported the volume at conservation pool elevation $320.0-\mathrm{ft} \mathrm{msl}$ to be $23,587 \mathrm{ac}$-ft with a surface area of 1,365 acres. The current survey measured 1,269 surface acres, or a difference of 96 surface acres.

Results indicate that the reservoir's volume at the conservation pool elevation of 320.0 ft is $20,242 \mathrm{ac}-\mathrm{ft}$. The total design volume of the reservoir was $23,587 \mathrm{ac}-\mathrm{ft}$; thus it appears that $3,345 \mathrm{ac}-\mathrm{ft}$ of volume have been lost to siltation.

Comparisons between the original design information and the 2001 data collection set is difficult and some apparent changes might simply be due to methodological differences. It is recommended that the similar survey be performed in five to ten years or after major flood events to monitor changes to the lake's storage volume.

| Year | 1975 (Original Design) | 2001 (TWDB Survey) |
| :--- | :---: | :---: |
| Area (acres) | 1,365 | 1,269 |
| Volume (acre-feet) | 23,587 | 20,242 |

Table 1. Area and volume comparisons at elevation 320.0 ft msl .

## REFERENCES

1. Camp Dresser \& McKee Consulting Engineers, Phase I Inspection Report National Dam Safety Program, 1979
2. Freese and Nichols Inc. Consulting Engineers, Safety Inspection of Swauano Creek Dam at Welsh Power Plant, September 1989

## Appendix A

Welsh Reservoir
RESERVOIR VOLUME TABLE
TEXAS WATER DEVELOPMENT BOARD

VOLUME IN ACRE-FEET
ELEVATION INCREMENT IS ONE TENTH FOOT

|  | VOLUME IN ACRE-FEET |  |  |  | ELEVATION INCREMENT IS ONE TENTH FOOT |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ELEVATION in Feet | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 276 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 277 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 278 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 279 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 |
| 280 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 |
| 281 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 |
| 282 | 4 | 4 | 4 | 5 | 5 | 5 | 6 | 7 | 8 | 9 |
| 283 | 10 | 11 | 13 | 15 | 16 | 18 | 21 | 23 | 26 | 28 |
| 284 | 31 | 34 | 37 | 41 | 44 | 47 | 51 | 55 | 59 | 63 |
| 285 | 68 | 72 | 77 | 82 | 88 | 93 | 99 | 105 | 112 | 119 |
| 286 | 126 | 133 | 140 | 148 | 156 | 164 | 173 | 181 | 190 | 199 |
| 287 | 208 | 218 | 228 | 238 | 248 | 259 | 270 | 281 | 292 | 303 |
| 288 | 315 | 327 | 339 | 351 | 363 | 376 | 389 | 402 | 415 | 428 |
| 289 | 442 | 456 | 470 | 484 | 499 | 514 | 529 | 544 | 560 | 576 |
| 290 | 593 | 610 | 626 | 644 | 661 | 679 | 698 | 716 | 735 | 755 |
| 291 | 775 | 795 | 815 | 836 | 857 | 879 | 900 | 923 | 945 | 968 |
| 292 | 992 | 1015 | 1039 | 1063 | 1087 | 1112 | 1137 | 1162 | 1188 | 1213 |
| 293 | 1239 | 1266 | 1292 | 1319 | 1346 | 1373 | 1401 | 1429 | 1457 | 1485 |
| 294 | 1514 | 1543 | 1572 | 1601 | 1630 | 1660 | 1690 | 1720 | 1750 | 1781 |
| 295 | 1811 | 1842 | 1873 | 1905 | 1936 | 1968 | 2000 | 2032 | 2065 | 2097 |
| 296 | 2130 | 2163 | 2197 | 2230 | 2264 | 2298 | 2332 | 2367 | 2401 | 2436 |
| 297 | 2471 | 2506 | 2541 | 2577 | 2613 | 2649 | 2685 | 2722 | 2759 | 2797 |
| 298 | 2834 | 2872 | 2911 | 2949 | 2988 | 3027 | 3067 | 3107 | 3147 | 3187 |
| 299 | 3228 | 3269 | 3311 | 3352 | 3394 | 3436 | 3479 | 3522 | 3565 | 3609 |
| 300 | 3653 | 3698 | 3742 | 3788 | 3833 | 3879 | 3925 | 3972 | 4019 | 4066 |
| 301 | 4114 | 4162 | 4211 | 4260 | 4309 | 4359 | 4409 | 4459 | 4510 | 4561 |
| 302 | 4613 | 4665 | 4718 | 4771 | 4824 | 4878 | 4932 | 4986 | 5041 | 5096 |
| 303 | 5151 | 5207 | 5263 | 5320 | 5376 | 5433 | 5491 | 5549 | 5607 | 5665 |
| 304 | 5724 | 5784 | 5843 | 5903 | 5963 | 6024 | 6084 | 6146 | 6207 | 6269 |
| 305 | 6331 | 6393 | 6456 | 6519 | 6582 | 6646 | 6710 | 6774 | 6839 | 6903 |
| 306 | 6969 | 7034 | 7100 | 7166 | 7232 | 7299 | 7366 | 7434 | 7502 | 7570 |
| 307 | 7638 | 7707 | 7776 | 7846 | 7915 | 7986 | 8056 | 8127 | 8198 | 8269 |
| 308 | 8341 | 8413 | 8485 | 8557 | 8630 | 8703 | 8777 | 8850 | 8924 | 8999 |
| 309 | 9073 | 9148 | 9224 | 9299 | 9375 | 9452 | 9528 | 9605 | 9682 | 9760 |
| 310 | 9838 | 9922 | 10007 | 10092 | 10177 | 10263 | 10349 | 10435 | 10522 | 10609 |
| 311 | 10696 | 10784 | 10873 | 10961 | 11050 | 11140 | 11229 | 11320 | 11410 | 11501 |
| 312 | 11592 | 11684 | 11776 | 11868 | 11961 | 12054 | 12147 | 12241 | 12335 | 12429 |
| 313 | 12524 | 12619 | 12715 | 12811 | 12907 | 13004 | 13101 | 13198 | 13296 | 13394 |
| 314 | 13493 | 13592 | 13691 | 13791 | 13891 | 13992 | 14093 | 14194 | 14296 | 14398 |
| 315 | 14500 | 14603 | 14707 | 14810 | 14915 | 15019 | 15125 | 15230 | 15336 | 15443 |
| 316 | 15550 | 15658 | 15766 | 15875 | 15984 | 16094 | 16204 | 16315 | 16426 | 16538 |
| 317 | 16651 | 16764 | 16877 | 16991 | 17106 | 17221 | 17337 | 17453 | 17569 | 17686 |
| 318 | 17804 | 17922 | 18040 | 18159 | 18278 | 18398 | 18518 | 18638 | 18759 | 18880 |
| 319 | 19002 | 19124 | 19247 | 19370 | 19493 | 19617 | 19741 | 19865 | 19990 | 20116 |
| 320 | 20242 |  |  |  |  |  |  |  |  |  |

## Appendix B

# Welsh Reservoir RESERVOIR AREA TABLE 

TEXAS WATER DEVELOPMENT BOARD
NOVEMBER 2001 SURVEY

| $\begin{gathered} \text { ELEVATION } \\ \text { in Feet } \\ \hline \end{gathered}$ | AREA IN ACRES |  |  |  | ELEVATION INCREMENT IS ONE TENTH FOOT |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 276 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 277 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 278 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 279 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 |
| 280 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 281 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 282 | 3 | 3 | 3 | 4 | 4 | 5 | 7 | 8 | 10 | 11 |
| 283 | 13 | 15 | 16 | 18 | 19 | 21 | 23 | 25 | 27 | 28 |
| 284 | 29 | 31 | 32 | 33 | 35 | 36 | 38 | 40 | 42 | 43 |
| 285 | 45 | 47 | 49 | 52 | 55 | 58 | 61 | 63 | 66 | 69 |
| 286 | 71 | 73 | 76 | 78 | 81 | 83 | 85 | 87 | 90 | 92 |
| 287 | 95 | 98 | 100 | 102 | 104 | 107 | 109 | 111 | 113 | 115 |
| 288 | 117 | 119 | 121 | 123 | 125 | 127 | 129 | 131 | 133 | 135 |
| 289 | 137 | 139 | 142 | 145 | 148 | 151 | 154 | 157 | 160 | 163 |
| 290 | 165 | 168 | 171 | 174 | 178 | 182 | 185 | 189 | 192 | 196 |
| 291 | 199 | 203 | 206 | 210 | 213 | 217 | 220 | 224 | 228 | 231 |
| 292 | 234 | 237 | 240 | 242 | 245 | 248 | 250 | 253 | 256 | 259 |
| 293 | 261 | 264 | 267 | 270 | 272 | 275 | 277 | 280 | 282 | 284 |
| 294 | 287 | 289 | 291 | 293 | 296 | 298 | 300 | 302 | 304 | 306 |
| 295 | 308 | 310 | 312 | 315 | 317 | 319 | 321 | 323 | 326 | 328 |
| 296 | 330 | 332 | 334 | 336 | 338 | 341 | 343 | 345 | 347 | 349 |
| 297 | 351 | 353 | 355 | 357 | 360 | 363 | 366 | 369 | 372 | 376 |
| 298 | 378 | 381 | 385 | 388 | 391 | 394 | 397 | 400 | 403 | 406 |
| 299 | 409 | 412 | 415 | 418 | 421 | 424 | 428 | 431 | 435 | 439 |
| 300 | 443 | 446 | 450 | 453 | 457 | 460 | 464 | 467 | 471 | 476 |
| 301 | 480 | 484 | 488 | 492 | 495 | 499 | 503 | 507 | 511 | 515 |
| 302 | 520 | 524 | 528 | 532 | 535 | 539 | 542 | 546 | 549 | 552 |
| 303 | 555 | 559 | 562 | 565 | 569 | 573 | 577 | 580 | 584 | 587 |
| 304 | 591 | 594 | 597 | 600 | 603 | 606 | 609 | 613 | 616 | 620 |
| 305 | 623 | 626 | 629 | 632 | 635 | 638 | 640 | 643 | 646 | 649 |
| 306 | 653 | 656 | 659 | 663 | 666 | 670 | 673 | 677 | 680 | 684 |
| 307 | 687 | 690 | 693 | 696 | 700 | 703 | 706 | 709 | 712 | 715 |
| 308 | 718 | 721 | 724 | 727 | 730 | 733 | 736 | 739 | 742 | 745 |
| 309 | 748 | 752 | 755 | 758 | 761 | 765 | 768 | 771 | 774 | 778 |
| 310 | 842 | 845 | 848 | 851 | 855 | 858 | 862 | 865 | 869 | 872 |
| 311 | 876 | 880 | 884 | 888 | 892 | 896 | 900 | 903 | 907 | 911 |
| 312 | 914 | 918 | 922 | 925 | 929 | 932 | 936 | 939 | 943 | 946 |
| 313 | 950 | 953 | 957 | 962 | 965 | 969 | 973 | 976 | 980 | 984 |
| 314 | 988 | 992 | 996 | 999 | 1003 | 1007 | 1011 | 1015 | 1019 | 1023 |
| 315 | 1027 | 1032 | 1036 | 1040 | 1045 | 1049 | 1054 | 1059 | 1064 | 1069 |
| 316 | 1074 | 1079 | 1084 | 1090 | 1095 | 1100 | 1106 | 1111 | 1116 | 1122 |
| 317 | 1127 | 1133 | 1138 | 1143 | 1148 | 1153 | 1158 | 1163 | 1168 | 1173 |
| 318 | 1177 | 1182 | 1186 | 1190 | 1194 | 1198 | 1202 | 1207 | 1211 | 1215 |
| 319 | 1219 | 1223 | 1227 | 1231 | 1235 | 1240 | 1244 | 1248 | 1252 | 1256 |
| 320 | 1269 |  |  |  |  |  |  |  |  |  |


-- - - - Pool Elevation 827.5' ———olume 2001

Welsh Reservoir
November 2001
Prepared by: TWDB
Appendix C Elevation vs. Volume



Appendix E
WELSH RESERVOIR
WELSH RESERVOIR

Appendix E



Appendix E

Appendix E

WELSH RESERVOIR

WELSH RESERVOIR

Appendix E

Appendix E

## Appendix F <br> Welsh Reservoir

## Range Line Endpoints

State Plane NAD83 Units-feet

| Range Line | X | Y |
| :---: | :---: | :---: |
| RL1-L | 3092332.4 | 7082864.8 |
| RL1-R | 3090851.7 | 7082547.5 |
| RL2-L | 3092303.6 | 7082999.4 |
| RL2-R | 3090899.8 | 7083850.3 |
| RL3-L | 3092679.6 | 7084853.5 |
| RL3-R | 3091262.8 | 7084833.5 |
| RL4-L | 3093174.0 | 7086667.6 |
| RL4-R | 3091462.3 | 7086927.1 |
| RL5-L | 3094082.4 | 7087912.6 |
| RL5-R | 3090755.6 | 7087917.5 |
| RL6-L | 3093025.1 | 7089394.8 |
| RL6-R | 3090623.4 | 7089886.1 |
| RL7-L | 3093851.6 | 7091388.5 |
| RL7-R | 3090909.4 | 7091008.7 |
| RL8-L | 3092380.5 | 7092974.9 |
| RL8-R | 3090342.2 | 7091878.8 |
| RL9-L | 3089442.2 | 7096793.2 |
| RL9-R | 3087839.9 | 7093929.2 |
| RL10-L | 3088041.8 | 7099376.1 |
| RL10-R | 3086320.7 | 7099395.3 |
| RL11-L | 3090789.2 | 7083835.9 |
| RL11-R | 3090621.0 | 7082850.4 |
| RL12-L | 3090332.5 | 7084234.9 |
| RL12-R | 3089779.7 | 7083725.3 |
| RL13-L | 3087851.9 | 7093604.7 |
| RL13-R | 3088140.3 | 7093066.3 |
| RL14-L | 3086818.3 | 7095263.3 |
| RL14-R | 3087001.0 | 7094147.9 |
| RL15-L | 3092890.1 | 7083658.0 |
| RL15-R | 3092683.1 | 7084748.0 |
| RL16-L | 3094194.2 | 7084071.4 |
| RL16-R | 3093493.8 | 7084727.7 |
| RL17-L | 3093649.7 | 7089042.4 |
| RL17-R | 3093463.2 | 7089360.0 |

## APPENDIX G - DEPTH SOUNDER ACCURACY

This example was extracted from the Innerspace Technology, Inc. Operation Manual for the Model 443 Velocity Profiler.

For the following examples,

$$
\mathrm{tD}=(\mathrm{D}-\mathrm{d}) / \mathrm{V}
$$

Where: $\mathrm{tD}=$ travel time of the sound pulse, in seconds (at depth $=\mathrm{D}$ )
$\mathrm{D}=$ depth, in feet
$\mathrm{d}=\mathrm{draft}=1.2$ feet
$\mathrm{V}=$ speed of sound, in feet per second

To calculate the error of a measurement based on differences in the actual versus average speed of sound, the same equation is used, in this format:

$$
D=[t(V)]+d
$$

For the water column from 2 to 30 feet: $\quad V=4832 \mathrm{fps}$ $\mathrm{t} 30=(30-1.2) / 4832=0.00596 \mathrm{sec}$.

For the water column from 2 to 45 feet: $\quad V=4808 \mathrm{fps}$ $\mathrm{t} 45=(45-1.2) / 4808=0.00911 \mathrm{sec}$.

For a measurement at 20 feet (within the 2 to 30 foot column with $V=4832 \mathrm{fps}$ ):
D20 $=[((20-1.2) / 4832)(4808)]+1.2=19.9^{\prime} \quad\left(-0.1^{\prime}\right)$
For a measurement at 30 feet (within the 2 to 30 foot column with $V=4832 \mathrm{fps}$ ):

$$
\begin{aligned}
\mathrm{D} 30 & =[((30-1.2) / 4832)(4808)]+1.2 \\
& =29.9^{\prime} \quad\left(-0.1^{\prime}\right)
\end{aligned}
$$

For a measurement at 50 feet (within the 2 to 60 foot column with $V=4799 \mathrm{fps}$ ):

$$
\begin{aligned}
\mathrm{D} 50 & =[((50-1.2) / 4799)(4808)]+1.2 \\
& =50.1^{\prime} \quad\left(+0.1^{\prime}\right)
\end{aligned}
$$

For the water column from 2 to 60 feet: $\quad V=4799 \mathrm{fps} \quad$ Assumed $\mathrm{V} 80=4785$ fps

$$
\begin{aligned}
\mathrm{t} 60 & =(60-1.2) / 4799 \\
& =0.01225 \mathrm{sec} .
\end{aligned}
$$

For a measurement at 10 feet (within the 2 to 30 foot column with $\mathrm{V}=4832 \mathrm{fps}$ ):

$$
\begin{aligned}
\mathrm{D} 10 & =[((10-1.2) / 4832)(4799)]+1.2 \\
& =9.9^{\prime} \quad\left(-0.1^{\prime}\right)
\end{aligned}
$$

For a measurement at 30 feet (within the 2 to 30 foot column with $\mathrm{V}=4832 \mathrm{fps}$ ):

$$
\begin{aligned}
\mathrm{D} 30 & =[((30-1.2) / 4832)(4799)]+1.2 \\
& =29.8^{\prime} \quad\left(-0.2^{\prime}\right)
\end{aligned}
$$

For a measurement at 45 feet (within the 2 to 45 foot column with $\mathrm{V}=4808 \mathrm{fps}$ ):

$$
\begin{aligned}
\mathrm{D} 45 & =[((45-1.2) / 4808)(4799)]+1.2 \\
& =44.9^{\prime} \quad\left(-0.1^{\prime}\right)
\end{aligned}
$$

For a measurement at 80 feet (outside the 2 to 60 foot column, assumed $V=4785 \mathrm{fps}$ ):

$$
\begin{aligned}
\mathrm{D} 80 & =[((80-1.2) / 4785)(4799)]+1.2 \\
& =80.2^{\prime} \quad\left(+0.2^{\prime}\right)
\end{aligned}
$$

Figure 1
WELSH RESERVOIR
Location Map



TWDB Survey November 2001


TWDB Survey November 2001


