## VOLUMETRIC SURVEY OF LAKE MONTICELLO

**Prepared for:** 

Titus County Fresh Water Supply District No. 1 In cooperation with Texas Utilities Electric Company



**Prepared by:** 

The Texas Water Development Board

March 10, 2003

## **Texas Water Development Board**

Craig D. Pedersen, Executive Administrator

#### **Texas Water Development Board**

William B. Madden, Chairman Elaine M. Barrón, M.D Charles L. Geren Noe Fernandez, Vice-Chairman Jack Hunt Wales H. Madden Jr.

Authorization for use or reproduction of any original material contained in this publication, i.e. not obtained from other sources, is freely granted. The Board would appreciate acknowledgment.

This report was prepared by the Hydrographic Survey group:

Scot Sullivan, P.E. Duane Thomas Wayne Elliott Priscilla Hays

For more information, please call (512) 936-0848

Published and Distributed by the Texas Water Development Board P.O. Box 13231 Austin, Texas 78711-3231

#### **TABLE OF CONTENTS**

INTRODUCTION	1
HISTORY AND GENERAL INFORMATION OF THE RESERVOIR	1
HYDROGRAPHIC SURVEYING TECHNOLOGY	2
GPS Information	2
Equipment and Methodology	4
Previous Survey Procedures	5
PRE-SURVEY PROCEDURES	6
SURVEY PROCEDURES	7
Equipment Calibration and Operation	7
Field Survey	8
Data Processing	9
RESULTS	11
SUMMARY	11

#### APPENDICES

APPENDIX A - DEPTH SOUNDER ACCURACY APPENDIX B - LAKE MONTICELLO VOLUME TABLE APPENDIX C - LAKE MONTICELLO AREA TABLE APPENDIX D - LAKE MONTICELLO AREA-ELEVATION-CAPACITY GRAPH APPENDIX E - CROSS-SECTION PLOTS

#### LIST OF FIGURES

FIGURE 1 - LOCATION MAP FIGURE 2 - LOCATION OF SURVEY DATA FIGURE 3 - SHADED RELIEF FIGURE 4 - DEPTH CONTOURS FIGURE 5 - 2-D CONTOUR MAP

### LAKE MONTICELLO HYDROGRAPHIC SURVEY REPORT

#### **INTRODUCTION**

Staff of the Hydrographic Survey Unit of the Texas Water Development Board (TWDB) conducted a hydrographic survey of Lake Monticello during the periods of February 19 and 24, 1998. The purpose of the survey was to determine the capacity of the lake at the conservation pool elevation. From this information, future surveys will be able to determine the location and rates of sediment deposition in the conservation pool over time. Survey results are presented in the following pages in both graphical and tabular form. All elevations presented in this report will be reported in feet above mean sea level based on the National Geodetic Vertical Datum of 1929 (NGVD '29) unless the elevation is noted otherwise. The conservation pool elevation for Lake Monticello is 340.0 feet. The design information/field survey estimates the original surface area at this elevation to be 2,000 acres and the storage volume to be 40,100 acre-feet of water.

#### HISTORY AND GENERAL INFORMATION OF THE RESERVOIR

Lake Monticello and Monticello Dam are owned and operated by Texas Utilities Electric Company. The reservoir is located on Blundell Creek in Titus County, two and one-half miles east of Monticello, Texas (see Figure 1). Records indicate the drainage area is approximately 36 square miles. At the conservation pool elevation, the lake has approximately 23.2 miles of shoreline and is 5.3 miles long. The widest point of the reservoir is approximately 1.1 miles (located 1.3 miles upstream of the dam).

The Texas Water Commission issued Permit No. 2591 on July 24, 1970 to Texas Utilities Electric Company. This original permit authorized the construction of a dam and to impound 40,100 acre-feet of water. The permit authorized consumptive use not to exceed 16,300 acre-feet per annum for the development of thermal electric power. This original permit was amended and later granted on July 6, 1973. Permit No. 2591A authorizes consumptive use not to exceed 15,300 acre-feet of

water per annum and 1,000 acre-feet of water per annum for industrial purposes associated with dust suppression and plant use at the Monticello mining site seven miles north of the reservoir. A certificate of Adjudication was issued to Texas Utilities Electric Company on October 13, 1986. Certificate of Adjudication No. 04-4563 authorized Texas Utilities Electric Company the impoundment capacities and water uses as stated in Permit No. 2591A.

Records indicate the construction for Lake Monticello and Monticello Dam began April 16, 1971 and deliberate impoundment began August 9, 1972. The project was officially completed in the spring of 1973. The design engineer was Forrest and Cotton Inc. and the general contractor was List and Clark Construction Company. The estimated cost of the dam was \$4,500,000.

Monticello Dam and appurtenant structures consist of a rolled earth fill embankment, approximately 3,200 feet in length. The embankment rises 54 feet above the natural streambed to an elevation of 352.0 feet. The service spillway is located at the left (east) abutment and is a concrete chute with an ogee crest. The crest is 160 feet in net length at elevation 328.0 feet. Four tainter gates, each 14 feet tall and 40 feet wide, control the service spillway. The emergency spillway, located to the right (west) of the dam, is an earth trench cut through the natural ground. The uncontrolled broad-crested weir is 1,000 feet in length at elevation 343.5 feet.

#### HYDROGRAPHIC SURVEYING TECHNOLOGY

The following sections will describe the theory behind Global Positioning System (GPS) technology and its accuracy. Equipment and methodology used to conduct the subject survey and previous hydrographic surveys are also addressed.

#### **GPS Information**

The following is a brief and simple description of Global Positioning System (GPS) technology. GPS is a relatively new technology that uses a network of satellites, maintained in precise

orbits around the earth, to determine locations on the surface of the earth. GPS receivers continuously monitor the broadcasts from the satellites to determine the position of the receiver. With only one satellite being monitored, the point in question could be located anywhere on a sphere surrounding the satellite with a radius of the distance measured. The observation of two satellites decreases the possible location to a finite number of points on a circle where the two spheres intersect. With a third satellite observation, the unknown location is reduced to two points where all three spheres intersect. One of these points is obviously in error because its location is in space, and it is ignored. Although three satellite measurements can fairly accurately locate a point on the earth, the minimum number of satellites required to determine a three dimensional position within the required accuracy is four. The fourth measurement compensates for any time discrepancies between the clock on board the satellites and the clock within the GPS receiver.

The United States Air Force and the defense establishment developed GPS technology in the 1960's. After program funding in the early 1970's, the initial satellite was launched on February 22, 1978. A four-year delay in the launching program occurred after the Challenger space shuttle disaster. In 1989, the launch schedule was resumed. Full operational capability was reached on April 27, 1995 when the NAVSTAR (NAVigation System with Time And Ranging) satellite constellation was composed of 24 Block II satellites. Initial operational capability, a full constellation of 24 satellites, in a combination of Block I (prototype) and Block II satellites, was achieved December 8, 1993. The NAVSTAR satellites provide data based on the World Geodetic System (WGS '84) spherical datum. WGS '84 is essentially identical to the 1983 North American Datum (NAD '83).

The United States Department of Defense (DOD) is currently responsible for implementing and maintaining the satellite constellation. In an attempt to discourage the use of these survey units as a guidance tool by hostile forces, the DOD has implemented means of false signal projection called Selective Availability (S/A). Positions determined by a single receiver when S/A is active result in errors to the actual position of up to 100 meters. These errors can be reduced to centimeters by performing a static survey with two GPS receivers, one of, which is set over a point with known coordinates. The errors induced by S/A are time-constant. By monitoring the movements of the satellites over time (one to three hours), the errors can be minimized during post processing of the collected data and the unknown position computed accurately. Differential GPS (DGPS) is an advance mode of satellite surveying in which positions of moving objects can be determine in real-time or "on-the-fly." This technological breakthrough was the backbone of the development of the TWDB's Hydrographic Survey Program. In the early stages of the program, one GPS receiver was set up over a benchmark with known coordinates established by the hydrographic survey crew. This receiver remained stationary during the survey and monitored the movements of the satellites overhead. Position corrections were determined and transmitted via a radio link once per second to another GPS receiver located on the moving boat. The boat receiver used these corrections, or differences, in combination with the satellite information it received to determine its differential location. This type of operation can obtain a horizontal positional accuracy of within one meter. In addition, the large positional errors experienced by a single receiver when S/A is active are negated. Since a greater accuracy is needed in the vertical direction, the depth sounder supplies vertical data during a survey. The lake surface during the survey serves as the vertical datum for the readings from the depth sounder.

The need for setting up a stationary shore receiver for current surveys has been eliminated by registration with a fee-based satellite reference position network (OmniSTAR). This service works in a differential mode basically the same way as the shore station, except on a worldwide basis. For a given area in the world, a network of several monitoring sites (with known positions) collect GPS signals from the NAVSTAR network. GPS corrections are computed at each of these sites to correct the GPS signal received to the known coordinates of the site. The corrections from each of the sites within the network are automatically sent via a leased line to a "Network Control Center" where the data corrections are checked and repackaged for up-link to a "Geostationary" L-band satellite. The "real-time" corrections for the entire given area in the world are then broadcast by the satellite to users of the system in the area covered by the satellite. The OmniSTAR receiver translates the information and supplies it to the on-board Trimble receiver for correction of the boat's GPS positions. The accuracy of this system in a real-time mode is normally one meter or less.

#### **Equipment and Methodology**

The equipment used in the performance of the hydrographic survey consisted of a 23-foot

aluminum tri-hull SeaArk craft with cabin, equipped with twin 90-Horsepower Johnson outboard motors. Installed within the enclosed cabin are an Innerspace Helmsman Display (for navigation), an Innerspace Technology Model 449 Depth Sounder and Model 443 Velocity Profiler, a Trimble Navigation, Inc. 4000SE GPS receiver, an OmniSTAR receiver, and an on-board 486 computer. A water-cooled generator through an in-line uninterruptible power supply provided electric power. Reference to brand names does not imply endorsement by the TWDB.

The GPS equipment, survey vessel, and depth sounder combine together to provide an efficient hydrographic survey system. As the boat travels across the lake surface, the depth sounder gathers approximately ten readings of the lake bottom each second. The depth readings are stored on the survey vessel's on-board computer along with the corrected positional data generated by the boat's GPS receiver. The daily data files collected are downloaded from the computer and brought to the office for editing after the survey is completed. During editing, bad data is removed or corrected, multiple data points are averaged to get one data point per second, and average depths are converted to elevation readings based on the daily-recorded lake elevation on the day the survey was performed. Accurate estimates of the lake volume can be quickly determined by building a 3-D model of the reservoir from the collected data. The level of accuracy is equivalent to or better than previous methods used to determine lake volumes, some of which are discussed below.

#### **Previous Survey Procedures**

Originally, reservoir surveys were conducted with a rope stretched across the reservoir along pre-determined range lines. A small boat would manually pole the depth at selected intervals along the rope. Over time, aircraft cable replaced the rope and electronic depth sounders replaced the pole. The boat was hooked to the cable, and depths were again recorded at selected intervals. This method, used mainly by the Soil Conservation Service, worked well for small reservoirs.

Larger bodies of water required more involved means to accomplish the survey, mainly due to increased size. Cables could not be stretched across the body of water, so surveying instruments were utilized to determine the path of the boat. Monumentation was set for the end points of each line so the same lines could be used on subsequent surveys. Prior to a survey, each end point had to be located (and sometimes reestablished) in the field and vegetation cleared so that line of sight could be maintained. One surveyor monitored the path of the boat and issued commands via radio to insure that it remained on line while a second surveyor determined depth measurement locations by turning angles. Since it took a major effort to determine each of the points along the line, the depth readings were spaced quite a distance apart. Another major cost was the land surveying required prior to the reservoir survey to locate the range line monuments and clear vegetation.

Electronic positioning systems were the next improvement. If triangulation could determine the boat location by electronic means, then the boat could take continuous depth soundings. A set of microwave transmitters positioned around the lake at known coordinates would allow the boat to receive data and calculate its position. Line of site was required, and the configuration of the transmitters had to be such that the boat remained within the angles of 30 and 150 degrees with respect to the shore stations. The maximum range of most of these systems was about 20 miles. Each shore station had to be accurately located by survey, and the location monumented for future use. Any errors in the land surveying resulted in significant errors that were difficult to detect. Large reservoirs required multiple shore stations and a crew to move the shore stations to the next location as the survey progressed. Land surveying remained a major cost with this method.

More recently, aerial photography has been used prior to construction, to generate elevation contours from which to calculate the volume of the reservoir. Fairly accurate results could be obtained, although the vertical accuracy of the aerial topography was generally one-half of the contour interval or  $\pm$  five feet for a ten-foot contour interval. This method could be quite costly and was only applicable in areas that were not inundated.

#### **PRE-SURVEY PROCEDURES**

The reservoir's surface area was determined prior to the survey by digitizing with AutoCad software the 740-foot contour. The boundary file was created from the 7.5-minute USGS quadrangle maps, WINFIELD, TX. 1965; and MONTICELLO, TX. 1965. The graphic boundary file created was then transformed into the proper datum, from NAD '27 datum to NAD '83, using Environmental

Systems Research Institute's (ESRI) Arc/Info project command with the NADCOM parameters. The area of the lake boundary was checked to verify that the area was the same in both datums.

The survey layout was designed by placing survey track lines at 500-foot intervals across the lake. The survey design for this lake required approximately 57 survey lines to be placed along the length of the lake. Survey setup files were created using Coastal Oceangraphics, Inc. Hypack software for each group of track lines that represented a specific section of the lake. The setup files were copied onto diskettes for use during the field survey.

#### SURVEY PROCEDURES

The following procedures were followed during the hydrographic survey of Lake Monticello performed by the TWDB. Information regarding equipment calibration and operation, the field survey, and data processing is presented.

#### **Equipment Calibration and Operation**

At the beginning of each surveying day, the depth sounder was calibrated with the Innerspace Velocity Profiler. The Velocity Profiler calculates an average speed of sound through the water column of interest for a designated draft value of the boat (draft is the vertical distance that the boat penetrates the water surface). The draft of the boat was previously determined to average 1.2 ft. The velocity profiler probe is placed in the water to moisten and acclimate the probe. The probe is then raised to the water surface where the depth is zeroed. The probe is lowered on a cable to just below the maximum depth set for the water column, and then raised to the surface. The unit displays an average speed of sound for a given water depth and draft, which is entered into the depth sounder. The depth value on the depth sounder was then checked manually with a measuring tape to ensure that the depth sounder was properly calibrated and operating correctly. During the survey of Lake Monticello, the speed of sound in the water column was determined to be 4,865 feet per second. Based on the measured speed of sound for various depths, and the average speed of sound calculated for the entire water column, the depth sounder is accurate to within  $\pm 0.2$  feet, plus an estimated error of  $\pm 0.3$  feet

due to the plane of the boat for a total accuracy of  $\pm 0.5$  feet for any instantaneous reading. These errors tend to be minimized over the entire survey, since some are positive and some are negative readings. Further information on these calculations is presented in Appendix A.

During the survey, the onboard GPS receiver was set to a horizontal mask of 10° and a PDOP (Position Dilution of Precision) limit of 7 to maximize the accuracy of horizontal positions. An internal alarm sounds if the PDOP rises above seven to advise the field crew that the horizontal position has degraded to an unacceptable level. The lake's initialization file used by the Hypack data collection program was setup to convert the collected DGPS positions on the fly to state plane coordinates. Both sets of coordinates were then stored in the survey data file.

#### **Field Survey**

Data were collected at Lake Monticello on February 19, 1998 and February 24, 1998. Approximately 108,526 data points were collected over the 28 miles traveled along the 35 survey lines run (pre-planned, random, and parallel). These points were stored digitally on the boat's computer in 35 data files. Data were not collected in areas of shallow water (depths less than 3.0 feet) or with significant obstructions unless these areas represented a large amount of water. Random data lines were also collected parallel to the original streambed in the main body of the lake. Figure 2 shows the actual location of all data collection points. In addition, on February 24, eleven lines of data were collected above the Highway 127 bridge on Blundell, Outlet, and Smith Bays using a small boat outfitted with a recording depth sounder.

TWDB staff observed the land around the lake to be vary between flat and rolling hills and that development was limited to the area of the power plant. On the depth sounder, a steep slope was noted near both shorelines with a wide fairly level bottom channel in the middle. From the survey vessel, the crew could see that the water was fairly clear with minimal underwater vegetation and that the lake was mostly free of any navigational hazards such as standing trees or stumps. There was a large, marked sandbar located on the west side of the lake near the mouth of County Park Cove about 2.0 feet below the surface that the bottom of the boat plowed over. Another hazard was noted around the Texas Utilities Power Plant intake on the northeast shore about 2000 feet upstream of the dam,

there were cables extending into the lake about 100 feet, protecting the intakes from boat traffic. Staff could not collect data in that area. The TWDB survey vessel could also not go under the bridge at Highway 127 due to a vertical clearance limitation. In addition, the boat could not be moved by land to other side of side of the bridge because there were no access areas. Staff therefore collected data above this bridge on February 24 using a small boat outfitted with a recording depth sounder.

All of the collected data were stored in individual data files for each pre-plotted range line or random collection event. Each of these files is tagged with a unique file tag, representative of the lake being surveyed. At the end of each day, the data files were copied to diskettes, for future processing in the office.

#### **Data Processing**

The collected data were downloaded from diskettes onto the TWDB's computer network. Tape backups were made for future reference as needed. To process the data, the EDIT routine in the Hypack Program was run on each raw data file. Data points such as depth spikes or data with missing depth or positional information were deleted from the file. The depth information collected every 0.1 seconds was averaged to get one reading for each second of data collection. A correction for the lake elevation at the time of data collection was also applied to each file during the EDIT routine. During the survey, the water surface held steady at 340.3 feet. After all changes had been made to the raw data file, the edited file was saved with a different extension. The edited files were combined into a single X,Y,Z data file, representative of the lake, to be used with the GIS software to develop a model of the lake's bottom surface. In addition, the eleven lines collected using the recording depth sounder only, were digitized and converted to data points by incrementing each cross-section in 1 foot increments along both the X, Y and Z axes. This procedure was accomplished by running an Arc/Info script file developed by TWDB staff. The eleven lines converted into 20,929 data points.

The resulting data file was imported into the UNIX operating system used to run Environmental System Research Institute's (ESRI) Arc/Info GIS software and converted to a MASS points file. The MASS points and the boundary file were then used to create a Digital Terrain Model (DTM) of the reservoir's bottom surface using Arc/Info's TIN software module. The module builds an irregular triangulated network from the data points and the boundary file. This software uses a method known as Delauney's criteria for triangulation. A triangle is formed between three nonuniformly spaced points, including all points along the boundary. If there is another point within the triangle, additional triangles are created until all points lie on the vertex of a triangle. All of the data points are preserved for use in determining the solution of the model by using this method. The generated network of three-dimensional triangular planes represents the actual bottom surface. Once the triangulated irregular network (TIN) is formed, the software then calculates elevations along the triangle surface plane by solving the equations for elevation along each leg of the triangle. Information for the entire reservoir area can be determined from the triangulated irregular network created using this method of interpolation.

If data points were collected outside the boundary file, the boundary was modified to include the data points. The boundary file in areas of significant sedimentation was also downsized as deemed necessary based on the data points and the observations of the field crew. The resulting boundary shape was used to develop each of the map presentations of the lake in this report.

There were some areas where volume and area values could not be calculated by interpolation because of a lack of information within the reservoir. "Flat triangles" were drawn at these locations. Arc/Info does not use flat triangle areas in the volume or contouring features of the model. Approximately 8,153 additional points were required for interpolation and contouring of the entire lake surface at elevation 340.0. Volumes and areas were calculated from the TIN for the entire reservoir at one-tenth of a foot intervals. From elevation 336.0 to elevation 340.0, the surface areas and volumes of the lake were mathematically estimated. This was done first by distributing uniformly across each elevation increment; the surface areas digitized from USGS topographic maps. Volumes were then calculated in a 0.1 foot step method by adding to the existing volume, 0.1 of the existing area, and 0.5 of the difference between the existing area the area for the value being calculated. The computed area of lake at elevation 340.0 was 2,001 surface acres. The computed area was 1 surface acres more than originally calculated. The computed reservoir volume table is presented in Appendix B and the area table in Appendix C. An elevation-area-volume graph is presented in Appendix D.

Other presentations developed from the model include a shaded relief map and a shaded depth

range map. To develop these maps, the TIN was converted to a lattice using the TINLATTICE command and then to a polygon coverage using the LATTICEPOLY command. Using the POLYSHADE command, colors were assigned to the range of elevations represented by the polygons that varied from navy to yellow. The lower elevation was assigned the color of navy, and the 340.0 lake elevation was assigned the color of yellow. Different color shades were assigned to the intermediate depths. Figure 3 presents the resulting depth shaded representation of the lake. Figure 4 presents a similar version of the same map, using bands of color for selected depth intervals. The color increases in intensity from the shallow contour bands to the deep-water bands.

Linear filtration algorithms were then applied to the DTM smooth cartographic contours versus using the sharp-engineered contours. The resulting contour map of the bottom surface at twofoot intervals is presented in Figure 5.

#### RESULTS

Results from the 1998 TWDB survey indicate Lake Monticello encompasses 2,001 surface acres and contains a volume of 34,740 acre-feet at the conservation pool elevation of 340.0 feet. The shoreline at this elevation was calculated to be 23.2 miles. The deepest point of the lake, elevation 293.7 or 46.3 feet of depth was located approximately 520 feet northwest from the center of the dam. Since this is a cooling reservoir, there is no real dead storage level in the reservoir. Therefore the capacity calculated above is the official volume of the lake.

#### SUMMARY

Lake Monticello was formed in 1972. Initial storage calculations estimated the volume at the conservation pool elevation of 340.0 feet to be 40,100 acre-feet with a surface area of 2,000 acres.

On February 19 and 24, 1998, a hydrographic survey of Lake Monticello was performed by the Texas Water Development Board's Hydrographic Survey Program. The 1998 survey used technological advances such as differential global positioning system and geographical information system technology to build a model of the reservoir's bathemetry. These advances allowed a survey to be performed quickly and to collect significantly more data of the bathemetry of Lake Monticello than previous survey methods. Results indicate that the lake's capacity at the conservation pool elevation of 340.0 feet was 34,740 acre-feet and the area was 2,001 acres.

The estimated reduction in storage capacity at the conservation pool elevation of 340.0 feet since 1972 is 5,360 acre-feet or 206 acre-feet per year. The average annual deposition rate of sediment in the conservation pool of the reservoir can be estimated at 5.726 acre-feet per square mile of drainage area. (*Please note that this is just a mathematical estimate based on the difference between the original survey and the current survey. In reality, the calculated value is unreasonable and should not be used. An error in the original volume is more likely the reason there is such a large difference in storage over the 26 years of operation.)* 

It is difficult to compare the original design information and the TWDB performed survey because little is know about the original design method, the amount of data collected, and the method used to process the collected data. However, the TWDB considers the 1998 survey to be a significant improvement over previous survey procedures and recommends that the same methodology be used in five to ten years or after major flood events to monitor changes to the lake's storage capacity.

#### CALCULATION OF DEPTH SOUNDER ACCURACY

This methodology was extracted from the Innerspace Technology, Inc. Operation Manual for the Model 443 Velocity Profiler.

For the following examples, t = (D - d)/V

where:  $t_D$  = travel time of the sound pulse, in seconds (at depth = D) D = depth, in feet d = draft = 1.2 feet V = speed of sound, in feet per second

To calculate the error of a measurement based on differences in the actual versus average speed of sound, the same equation is used, in this format:

$$\mathsf{D} = [\mathsf{t}(\mathsf{V})] + \mathsf{d}$$

For the water column from 2 to 30 feet: V = 4832 fps

 $t_{30} = (30-1.2)/4832$ = 0.00596 sec.

For the water column from 2 to 45 feet: V = 4808 fps

 $t_{45} = (45 - 1.2)/4808$ = 0.00911 sec.

For a measurement at 20 feet (within the 2 to 30 foot column with V = 4832 fps):

 $D_{20} = [((20-1.2)/4832)(4808)] + 1.2$ = 19.9' (-0.1')

For a measurement at 30 feet (within the 2 to 30 foot column with V = 4832 fps):

$$D_{30} = [((30-1.2)/4832)(4808)] + 1.2$$
  
= 29.9' (-0.1')

For a measurement at 50 feet (within the 2 to 60 foot column with V = 4799 fps):

$$D_{50} = [((50-1.2)/4799)(4808)] + 1.2$$
  
= 50.1' (+0.1')

For the water column from 2 to 60 feet: V = 4799 fps Assumed  $V_{80} = 4785$  fps

$$t_{60} = (60-1.2)/4799$$
  
=0.01225 sec.

For a measurement at 10 feet (within the 2 to 30 foot column with V = 4832 fps):

$$D_{10} = [((10-1.2)/4832)(4799)] + 1.2$$
  
= 9.9' (-0.1')

For a measurement at 30 feet (within the 2 to 30 foot column with V = 4832 fps):

$$D_{30} = [((30-1.2)/4832)(4799)]+1.2$$
  
= 29.8' (-0.2')

For a measurement at 45 feet (within the 2 to 45 foot column with V = 4808 fps):

$$D_{45} = [((45-1.2)/4808)(4799)] + 1.2$$
  
= 44.9' (-0.1')

For a measurement at 80 feet (outside the 2 to 60 foot column, assumed V = 4785 fps):

$$D_{80} = [((80-1.2)/4785)(4799)] + 1.2$$
  
= 80.2' (+0.2')

#### TEXAS WATER DEVELOPMENT BOARD RESERVOIR VOLUME TABLE

#### Lake Monticello February 1998 Survey

		VOLUME IN ACRE-FEET			ELEVATION INCREMENT IS ONE TENTH FOOT						
ELEV.	FEET	.0	.1	.2	.3	-4	.5	.6	.7	.8	.9
294											
295											
296											
297											
298		1	1	1	1	1	1	1	1	2	2
299		3	3	4	5	6	7	9	11	13	15
300		18	21	25	28	32	36	41	45	50	56
301		61	67	73	80	86	93	100	108	116	124
302		132	141	150	159	169	179	189	200	210	222
303		233	244	256	268	280	293	305	318	331	345
304		358	372	386	401	415	430	446	462	478	495
305		512	529	547	565	583	602	622	641	662	683
306		704	726	748	770	793	817	840	865	889	914
307		940	965	992	1019	1046	1073	1101	1130	1158	1188
308		217	1247	1278	1308	1339	1371	1403	1435	1467	1500
309	1	534	1568	1602	1637	1673	1709	1745	1783	1820	1859
310	- 1	898	1938	1979	2020	2062	2104	2148	2191	2235	2280
311	2	325	2371	2417	2464	2511	2558	2607	2655	2704	2753
312	2	2803	2853	2904	2954	3006	3057	3109	3161	3214	3267
313	3	321	3375	3429	3485	3540	3597	3653	3710	3768	3826
314	3	885	3944	4003	4063	4124	4184	4245	4307	4369	4431
315	4	494	4557	4620	4684	4748	4812	4877	4942	5007	5073
316	5	5138	5204	5270	5337	5404	5470	5538	5605	5673	5741
317	5	5809	5877	5946	6014	6083	6153	6222	6292	6362	6433
318	6	504	6575	6647	6719	6791	6864	6937	7011	7085	7159
319	7	234	7310	7386	7462	7540	7618	7696	7776	7856	7936
320	8	3018	8100	8182	8266	8349	8434	8519	8604	8690	8777
321	8	3864	8951	9040	9128	9217	9307	9397	9488	9579	9671
322	5	763	9856	9949	10043	10137	10231	10327	10422	10518	10615
323	10	0712	10809	10907	11006	11105	11204	11304	11405	11506	11608
324	11	1710	11813	11916	12019	12123	12227	12332	12437	12542	12647
325	12	2753	12859	12965	13072	13179	13286	13394	13502	13610	13718
326	13	3827	13936	14046	14156	14267	14377	14489	14602	14715	14828
327	14	942	15057	15172	15287	15403	15520	15637	15756	15875	15994
328	16	5115	16235	16357	16478	16600	16722	16845	16968	17091	17215
329	17	7339	17463	17588	17713	17838	17964	18090	18217	18344	18471
330	18	3599	18727	18856	18985	19114	19244	19374	19505	19636	19768
331	15	9901	20034	20168	20302	20437	20573	20709	20845	20983	21121
332	21	1259	21399	21538	21679	21820	21961	22104	22246	22389	22533
333	22	2677	22822	22968	23114	23261	23408	23556	23705	23854	24003
334	24	¥153	24304	24456	24608	24760	24913	25067	25221	25376	25532
335	25	5688	25845	26003	26161	26320	26480	26640	26801	26963	27129
336	27	7296	27465	27634	27804	27975	28148	28320	28494	28669	28845
337	29	2021	29199	29377	29557	29737	29918	30100	30283	30467	30651
338	30	0837	31023	31211	31399	31588	31779	31970	32162	32355	32548
339	32	2743	32939	33135	33332	33531	33730	33930	34131	54333	54536
340	34	740									

#### TEXAS WATER DEVELOPMENT BOARD RESERVOIR AREA TABLE

Lake Monticello February 1998 Survey

		AREA IN ACRES				ELEVATION INCREMENT IS ONE TENTH FOOT				
ELEV. FEE	т.0	.1	.2	.3	- 4	.5	.6	.7	.8	.9
201										
294										
295										
290										
297	1	1	1	1	1	2	2	3	4	5
290	6	7	8	10	12	14	17	21	24	26
299	20	32	34	37	40	43	46	49	52	55
300	57	50	62	65	68	70	73	77	80	83
202	86	80	02	95	98	101	105	107	109	112
302	114	116	118	121	123	126	128	130	133	135
303	137	139	142	145	149	153	157	161	165	168
205	171	175	179	182	187	191	196	202	207	211
204	214	218	223	227	232	236	240	244	248	252
300	257	261	265	269	273	277	282	287	291	294
307	208	301	305	309	313	316	320	324	328	332
300	270	343	347	352	357	363	370	376	382	388
309	305	402	410	417	423	428	433	438	443	449
211	455	460	465	469	474	479	483	487	491	495
712	400	503	506	510	514	517	521	525	529	533
212	538	544	550	555	559	564	568	574	579	584
71/	580	503	597	601	605	610	614	617	621	625
314	620	632	635	639	642	645	648	651	653	656
316	658	661	663	666	668	671	673	675	678	680
317	682	684	687	689	692	694	697	700	704	707
318	711	714	718	722	726	730	734	738	743	747
319	752	757	763	770	777	784	791	797	804	810
320	817	823	829	835	841	848	853	858	862	867
321	872	878	883	889	894	900	905	910	915	920
322	924	929	934	939	944	949	954	958	963	967
323	972	977	982	988	993	999	1004	1009	1014	1019
324	1024	1028	1033	1037	1040	1043	1046	1050	1053	1056
325	1059	1062	1065	1068	1071	1074	1078	1081	1084	1087
326	1091	1094	1098	1102	1106	1118	1123	1127	1131	1136
327	1143	1148	1153	1158	1163	1173	1180	1186	1193	1200
328	1207	1210	1214	1217	1221	1224	1227	1231	1234	1238
329	1242	1245	1249	1253	1256	1260	1264	1267	1271	1275
330	1280	1284	1288	1292	1297	1301	1306	1310	1315	1321
331	1328	1335	1341	1347	1353	1359	1364	1370	1376	1382
332	1392	1397	1402	1407	1413	1418	1423	1428	1434	1439
333	1449	1454	1459	1465	1470	1476	1482	1488	1493	1499
334	1506	1511	1517	1522	1528	1534	1540	1546	1553	1559
335	1566	1573	1579	1586	1593	1601	1608	1615	1623	1630
336	1639	1648	1657	1666	1675	1684	1693	1702	1711	1721
337	1730	1739	1748	1757	1766	1775	1784	1793	1802	1811
338	1820	1829	1838	1847	1856	1865	1874	1883	1892	1902
339	1911	1920	1929	1938	1947	1956	1965	1974	1983	1992
340	2001									



# ELEVATION (Feet)



DISTANCE (Feet) PREPARED BY: TWDB MAY 1998

#### LAKE MONTICELLO Cross Section A-A'

#### LAKE MONTICELLO Cross Section B-B'



DISTANCE (Feet) PREPARED BY: TWDB MAY 1998



DISTANCE (Feet) PREPARED BY: TWDB MAY 1998

### LAKE MONTICELLO Cross Section D-D'



DISTANCE (Feet) PREPARED BY: TWDB MAY 1998

## PREPARED BY: TWDB MAY 1998





## FIGURE 2 LAKE MONTICELLO

#### Location of Survey Data



PREPARED BY: TEXAS WATER DEVELOPMENT BOARD MAY 1998

FIGURE 3 LAKE MONTICELLO Shaded Relief

1"= 2800'

ELEVATION IN FEET

	293.7 - 299.5
	299.5 - 304
	304 - 308.5
	308.5 - 313
and the second	313- 317.5
	317.5 - 322
	322 - 326.5
	326.5 - 331
	331 - 335.5
	335.5 - 340

## FIGURE 4 LAKE MONTICELLO Depth Ranges

N

1"= 2800'

EXPL	ANATION
	0 - 12'
	12 - 24'
	24 - 36'
	36 - 46.3'

PREPARED BY: TEXAS WATER DEVELOPMENT BOARD MAY 1998