# Volumetric and Sedimentation Survey of CHOKE CANYON RESERVOIR <br> June 2012 Survey 

# Texas Water <br> Development Board 

August 2013

# Texas Water Development Board 

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Prepared for:

## City of Corpus Christi

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## Texas Water Development Board

## Executive summary

In March 2012 the Texas Water Development Board (TWDB) entered into agreement with the City of Corpus Christi, Texas, to perform a volumetric and sedimentation survey of Choke Canyon Reservoir. Surveying was performed using a multi-frequency ( $200 \mathrm{kHz}, 50 \mathrm{kHz}$, and 24 kHz ), sub-bottom profiling depth sounder. In addition, sediment core samples were collected in select locations and correlated with the multi-frequency depth sounder signal returns to estimate sediment accumulation thicknesses and sedimentation rates.

Choke Canyon Dam and Choke Canyon Reservoir are located on the Frio River in Live Oak and McMullen Counties, approximately 3.5 miles northwest of the City of Three Rivers, Texas. The conservation pool elevation of Choke Canyon Reservoir is 220.5 feet (NGVD29). TWDB collected bathymetric data for Choke Canyon Reservoir between June 5, 2012, and June 27, 2012. The daily average water surface elevations during the survey ranged between 207.11 and 207.66 feet (NGVD29).

The 2012 TWDB volumetric survey indicates that Choke Canyon Reservoir has a total reservoir capacity of $\mathbf{6 6 2 , 8 2 1}$ acre-feet and encompasses $\mathbf{2 5 , 4 3 8}$ acres at conservation pool elevation (220.5 feet above mean sea level, NGVD29). Previous capacity estimates include the original design estimate of 691,130 acre-feet at the time of impoundment in 1982, an area-capacity table from the U.S. Bureau of Reclamation dated 1983 indicating a capacity of 695,125 acre-feet, and a 1993 TWDB volumetric survey estimate of 695, 271 acre-feet.

Based on two methods for estimating sedimentation rates, the 2012 TWDB sedimentation survey estimates Choke Canyon Reservoir loses between 944 and 1,708 acre-feet of capacity per year below conservation pool elevation ( 220.5 feet NGVD29) due to sedimentation. The sedimentation survey indicates sediment accumulation is somewhat consistent throughout the reservoir. The heaviest accumulations measured by this survey are within the submerged river channels. Accumulation in the Frio River channel becomes heavier as it approaches the dam. TWDB recommends that a similar methodology be used to resurvey Choke Canyon Reservoir in 10 years or after a major flood event.

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Note: References to brand names throughout this report do not imply endorsement by the Texas Water Development Board

## Introduction

The Hydrographic Survey Program of the Texas Water Development Board (TWDB) was authorized by the $72^{\text {nd }}$ Texas State Legislature in 1991. The Texas Water Code authorizes TWDB to perform surveys to determine reservoir storage capacity, sedimentation levels, rates of sedimentation, and projected water supply availability.

In March 2012 TWDB entered into agreement with the City of Corpus Christi, Texas, to perform a volumetric and sedimentation survey of Choke Canyon Reservoir (TWDB, 2012). This report describes the methods used to conduct the volumetric and sedimentation survey, including data collection and processing techniques. This report serves as the final contract deliverable from TWDB to the City of Corpus Christi, Texas and contains as deliverables: (1) an elevation-area-capacity table of the reservoir acceptable to the Texas Commission on Environmental Quality [Appendix A, B], (2) a bottom contour map [Figure 5], (3) a shaded relief plot of the reservoir bottom [Figure 3], and (4) an estimate of sediment accumulation and location [Figure 10].

## Choke Canyon Reservoir general information

Choke Canyon Dam and Choke Canyon Reservoir are located on the Frio River in Live Oak and McMullen Counties, approximately 3.5 miles northwest of Three Rivers, Texas, and approximately 80 miles south of San Antonio, Texas (TPWD, 2012) (Figure 1). Choke Canyon Dam and Choke Canyon Reservoir are owned by the U.S. Department of the Interior, Bureau of Reclamation, and operated by the City of Corpus Christi (COCC, 2013). Construction on Choke Canyon Dam began on August 10, 1978. The dam was considered substantially complete on May 18, 1982, and the official dedication ceremony was held on June 8, 1982 (USBR, 2013).

Choke Canyon Reservoir gets its name from the low-lying hills that force the confluence of the three rivers, the Frio, Nueces, and Atascosa Rivers, into a constricted channel. Choke Canyon Dam and Reservoir, in conjunction with Lake Corpus Christi, was built primarily as a water supply reservoir for the Cities of Corpus Christi and Three Rivers, and the Nueces River Authority, supplying water for municipal and industrial purposes, as well as recreational purposes (USBR, 2013). Additional pertinent data about Choke Canyon Dam and Choke Canyon Reservoir can be found in Table 1.

Water rights for Choke Canyon Reservoir have been appropriated to the City of Corpus Christi, the Nueces River Authority, and the City of Three Rivers through

Certificate of Adjudication No. 21-3214 and Amendment to Certificate of Adjudication No. $21-3214 \mathrm{~A}$. The complete certificates are on file in the Information Resources Division of the Texas Commission on Environmental Quality.


Figure 1. Location of Choke Canyon Reservoir

Table 1. Pertinent data for Choke Canyon Dam and Choke Canyon Reservoir
Owner
U.S. Department of the Interior, Bureau of Reclamation

Engineer (design)
U.S. Department of the Interior, Bureau of Reclamation

General contractor
Holloway Construction Company
Location of dam
On the Frio River in Live Oak County, approximately 3.5 miles northwest of Three Rivers, Texas
Dam

| Type | Rolled earthfill |
| :--- | :--- |
| Length (total) | 3.5 miles |
| Height | 114.14 feet |
| Crest elevation | 241.14 feet above mean sea level |

Spillway (service/ emergency)
Type Concrete ogee
Width 368 feet
Sill elevation $\quad 199.5$ feet above mean sea level
Control for water release $\quad 7$ radial gates each 49.2 feet by 23.7 feet
Top-of-gate elevation 223.2 feet above mean sea level

## Outlet works

The intake tower for the river outlet works is a concrete structure outfitted with four multilevel gates at elevations 203.0, 181.5, 150.0, and 136.38 feet
Reservoir data (Based on 2012 TWDB survey)

| Feature | Elevation <br> (feet NGVD29 |
| :--- | :--- | :--- | :--- |
| Top of dam |  |$\quad$| Capacity |
| :--- |
| (acre-feet) |$\quad$| Area |
| :--- |
| (acres) |

Source: (TWDB, 2003, USBR, 2012)
${ }^{\text {a }}$ NGVD29 $=$ National Geodetic Vertical Datum 1929
${ }^{\mathrm{b}}$ Conservation storage capacity equals total capacity at conservation pool elevation minus dead pool capacity. Dead pool refers to water that cannot be drained by gravity through a dam's outlet works.

## Volumetric and sedimentation survey of Choke Canyon Reservoir

## Datum

The vertical datum used during this survey is the National Geodetic Vertical Datum 1929 (NGVD29). This datum is also utilized by the United States Geological Survey (USGS) for the reservoir elevation gage USGS 08206900 Choke Canyon Res nr Three Rivers, TX (USGS, 2013). Elevations herein are reported in feet relative to the NGVD29 datum. Volume and area calculations in this report are referenced to water levels provided by the USGS gage. The horizontal datum used for this report is North American Datum 1983 (NAD83), and the horizontal coordinate system is State Plane Texas South Central Zone (feet).

## TWDB bathymetric and sedimentation data collection

TWDB collected bathymetric data for Choke Canyon Reservoir between June 5, 2012, and June 27, 2012. The daily average water surface elevations during the survey ranged between 207.11 and 207.66 feet (NGVD29). For data collection, TWDB used a Specialty Devices, Inc. (SDI), single-beam, multi-frequency ( $200 \mathrm{kHz}, 50 \mathrm{kHz}$, and 24 kHz ) sub-bottom profiling depth sounder integrated with differential global positioning system (DGPS) equipment. Data collection occurred while navigating along pre-planned survey lines oriented perpendicular to the assumed location of the original river channels and spaced approximately 500 feet apart. Many of the survey lines were also surveyed by TWDB during the 1993 survey. The depth sounder was calibrated daily using a velocity profiler to measure the speed of sound in the water column and a weighted tape or stadia rod for depth reading verification. Figure 2 shows where data collection occurred during the 2012 TWDB survey.

All sounding data was collected and reviewed before sediment core sampling sites were selected. Sediment core samples are collected at regularly spaced intervals within the reservoir, or at locations where interpretation of the acoustic display would be difficult without site-specific sediment core data. Following the analysis of the sounding data, TWDB selected eight locations to collect sediment core samples (Figure 2). The sediment core samples were collected on June 17, 2013, with a custom-coring boat and SDI VibeCore system.

Sediment cores are collected in 3-inch diameter aluminum tubes. Analysis of the acoustic data collected during the bathymetric survey assists in determining the depth of penetration the tube must be driven during sediment sampling. The goal is to collect a sediment core sample extending from the current reservoir-bottom, through the accumulated sediment, and to the pre-impoundment surface. After retrieving the sample, a stadia rod is inserted into the top of the tube to assist in locating the top of the sediment in the tube. This identifies the location of the layer corresponding to the current reservoir surface. The aluminum tube is cut to this level, capped, and transported back to TWDB headquarters for further analysis. During this time, some settling of the upper layer can occur.


Figure 2. Data collected during 2012 TWDB Choke Canyon Reservoir survey

## Data processing

## Model boundaries

The reservoir boundary was determined using multiple sources. For the portion of the boundary at conservation pool elevation within Live Oak County, the boundary was digitized from aerial photographs, also known as digital orthophoto quarter-quadrangle images (DOQQs), obtained from the Texas Natural Resources Information System (TNIRIS, 2009) using Environmental Systems Research Institute's ArcGIS software. The quarter-quadrangles that cover Choke Canyon Reservoir in Live Oak County are Three Rivers (NW), Willow Hollow Tank (SW, SE), and Calliham (NW, NE).The DOQQs were photographed on October 11, 2004, while the daily average water surface elevation measured 220.53 feet (NGVD29). The 2004 DOQQs have a resolution or ground sample distance of 1.0 -meters and a horizontal accuracy within $\pm 5$ meters to existing mosaicked digital orthorectified imagery (USDA, 2013). For this analysis, the boundary was digitized at the land-water interface in the 2004 photographs and given an elevation of 220.5 feet for modeling purposes. The portion of the boundary at conservation pool elevation within McMullen County was extracted from a raster created using Light Detection and Ranging (LIDAR) data. The LIDAR data for McMullen County was collected between June 17, 2009, and July 15 , 2009, while the daily average water surface elevation of the reservoir measured between 212.36 feet and 213.1 feet above mean sea level. More information
about the LIDAR data and how it was used in the reservoir model can be found in the section on LIDAR below.

Additional boundary information was obtained from aerial photographs taken on April 24, 2010, while the water surface elevation measured 216.78 feet, and May 22, 2012, while the water surface elevation measured 207.98 feet. Contours were digitized at the land-water interface in the photos and added to the model as point data. A boundary at elevation 216.78 feet was added only to the Live Oak County part of the reservoir where LIDAR data is unavailable. The contour at elevation 207.98 feet was digitized for the entire reservoir. According to metadata associated with the 2010 and 2012 DOQQs, the photographs have a resolution or ground sample distance of 1.0-meters and a horizontal accuracy within $\pm 6$ meters to true ground (USDA, 2013, TNRIS 2010, TNRIS, 2012).

## LIDAR

Light Detection and Ranging Data is available from the Texas Natural Resource Information System (TNRIS, 2013). LIDAR for McMullen County was collected between June 17, 2009, and July 15, 2009. The daily average water surface elevation of the reservoir during this period varied between 212.36 feet and 213.1 feet above mean sea level during this time. The LIDAR data was used to generate a boundary for the reservoir at conservation pool elevation in McMullen County and to add additional LIDAR points within the boundary. To generate the boundary, LIDAR data with a classification equal to 2, or ground, was imported into an ArcGIS file geodatabase from .las files. A topographical model of the data was generated and converted to a raster using a cell size of 5 meters by 5 meters. The horizontal datum of the LIDAR data is Universal Transverse Mercator (UTM) North American Datum 1983 (NAD83) Zone 14 and the vertical datum is North American Vertical Datum 1988 (NAVD88). According to the associated metadata, the LIDAR data has a vertical accuracy of $\pm 18$ centimeters.

To make the LIDAR data compatible with the bathymetric survey data, it was necessary to transform the LIDAR data to NGVD29 (vertical) and NAD83 (horizontal) coordinates. Horizontal coordinate transformations were done using the ArcGIS Project tool. Vertical coordinate transformations were done by applying a single vertical offset to all LIDAR data. The offset was determined by applying the National Oceanic and Atmospheric Administration National Geodetic Survey's NADCON software (NGS, 2013a) and VERTCON software (NGS, 2013b) to single reference point in the vicinity of
the survey, the reservoir elevation gage USGS 08206900 Choke Canyon Res nr Three Rivers, $T X$, of Latitude $28^{\circ} 29^{\prime} 01^{\prime \prime}$, Longitude $98^{\circ} 14^{\prime} 44^{\prime \prime}$ NAD27. The resulting conversion factor of 0.026 meters was subtracted from all LIDAR data elevations to obtain the transformed vertical elevations.

To reduce computational burden, the LIDAR data was filtered to include only every $10^{\text {th }}$ point before clipping to include only data points within the reservoir boundary. The LIDAR data points have an average spacing of 0.6 meters; therefore, using a thinned point dataset did not significantly affect the modeled topography of the coverage area. No interpolation of the data in the areas of LIDAR coverage was necessary. After the points were clipped to within the boundary, the shapefile was projected to NAD83 State Plane Texas South Central Zone (feet), and new attribute fields were added to first convert the elevations from meters NAVD88 to meters NGVD29, then to feet NGVD29.

## Triangulated Irregular Network model

Following completion of data collection, the raw data files collected by TWDB were edited to remove data anomalies. DepthPic©, software developed by SDI, Inc., is used to display, interpret, and edit the multi-frequency data by manually removing data anomalies in the current bottom surface and manually digitizing the reservoir-bottom surface at the time of initial impoundment (i.e. pre-impoundment surface). For processing outside of DepthPic©, an in-house software package, HydroTools, is used to identify the current reservoir-bottom surface, pre-impoundment surface, sediment thickness at each sounding location, and output the data into a single file. The water surface elevation at the time of each sounding was used to convert each sounding depth to a corresponding reservoir-bottom elevation. This survey point dataset is then preconditioned by inserting a uniform grid of artificial survey points between the actual survey lines. Bathymetric elevations at these artificial points are determined using an anisotropic spatial interpolation algorithm described in the spatial interpolation of reservoir bathymetry section below. This technique creates a high resolution, uniform grid of interpolated bathymetric elevation points throughout a majority of the reservoir (McEwen et al., 2011). Finally, the point file resulting from spatial interpolation is used in conjunction with sounding and boundary data to create volumetric and sediment Triangulated Irregular Network (TIN) models utilizing the 3D Analyst Extension of ArcGIS. The 3D Analyst algorithm uses Delaunay's criteria
for triangulation to create a grid composed of triangles from non-uniformly spaced points, including the boundary vertices (ESRI, 1995).

## Spatial interpolation of reservoir bathymetry

Isotropic spatial interpolation techniques such as the Delaunay triangulation used by the 3D Analyst extension of ArcGIS are, in many instances, unable to suitably interpolate bathymetries between survey lines common to reservoir surveys. Reservoirs and stream channels are anisotropic morphological features where bathymetry at any particular location is more similar to upstream and downstream locations than to transverse locations. Interpolation schemes that do not consider this anisotropy lead to the creation of several types of artifacts in the final representation of the reservoir bottom surface and hence to errors in volume. These include: artificially-curved contour lines extending into the reservoir where the reservoir walls are steep or the reservoir is relatively narrow; intermittent representation of submerged stream channel connectivity; and oscillations of contour lines in between survey lines. These artifacts reduce the accuracy of the resulting volumetric and sediment TIN models in areas between actual survey data.

To improve the accuracy of bathymetric representation between survey lines, TWDB developed various anisotropic spatial interpolation techniques. Generally, the directionality of interpolation at different locations of a reservoir can be determined from external data sources. A basic assumption is that the reservoir profile in the vicinity of a particular location has upstream and downstream similarity. In addition, the sinuosity and directionality of submerged stream channels can be determined from direct examination of survey data or more robustly by examining scanned USGS 7.5 minute quadrangle maps (known as digital raster graphics) and hypsography files (the vector format of USGS 7.5 minute quadrangle map contours), when available. Using the survey data, polygons are created to partition the reservoir into segments with centerlines defining directionality of interpolation within each segment. For surveys with similar spatial coverage, these interpolation definition files are in principle independent of the survey data and could be applied to past and future survey data of the same reservoir. In practice, however, minor revisions of the interpolation definition files may be needed to account for differences in spatial coverage and boundary conditions between surveys. Using the interpolation definition files and survey data, the current reservoir-bottom elevation, pre-impoundment elevation, and sediment thickness are calculated for each point in the high resolution
uniform grid of artificial survey points. The reservoir boundary, artificial survey points grid, and survey data points are used to create volumetric and sediment TIN models representing the reservoir bathymetry and sediment accumulation throughout the reservoir. Specific details of this interpolation technique can be found in the HydroTools manual (McEwen et al., 2011a) and in McEwen et al., 2011b.

In areas inaccessible to survey data collection such as small coves and shallow upstream areas of the reservoir, linear extrapolation is used for volumetric and sediment accumulation estimations. The linear extrapolation follows a linear definition file linking the survey points file to the lake boundary file (McEwen et al., 2011a). Without extrapolated data, the TIN Model builds flat triangles. A flat triangle is defined as a triangle where all three vertices are equal in elevation, generally the elevation of the reservoir boundary. Reducing flat triangles, by applying linear extrapolation, improves the elevationcapacity and elevation-area calculations. It may not be possible to remove all flat triangles, and linear extrapolation is only applied where adding bathymetry is deemed reasonable. For example, linear extrapolation was deemed reasonable and applied to Choke Canyon Reservoir in the following situations: in small coves of the main body of the reservoir and in obvious channel features. Linear extrapolation was applied up to the conservation pool elevation boundary in the Live Oak County portion of the reservoir only. To reduce flat triangles at elevation 207.98 feet, the contour elevation from the 2012 DOQQs, linear extrapolation was applied up to the 2012 boundary in McMullen County (Figure 3).

Figure 3 illustrates typical results from application of the anisotropic interpolation and linear extrapolation techniques to Choke Canyon Reservoir. In Figure 3A, deeper channels indicated by surveyed cross sections are not continuously represented in areas between survey cross sections. This is an artifact of the TIN generation routine rather than an accurate representation of the physical bathymetric surface. Inclusion of interpolation points, represented in Figure 3C, in creation of the volumetric TIN model directs Delaunay triangulation to better represent the reservoir bathymetry between survey cross-sections. The bathymetry shown in Figure 3C was used in computing reservoir capacity and area tables (Appendix A, B).


Figure 3. Anisotropic spatial interpolation and linear extrapolation of Choke Canyon Reservoir sounding data - A) bathymetric contours without interpolated points, B) sounding points(black) and interpolated points (red), C) bathymetric contours with the interpolated points

## Area, volume, and contour calculations

Using ArcInfo software and the volumetric TIN model, volumes and areas were calculated for the entire reservoir at 0.1 feet intervals, from elevation 135.3 to 220.5 feet. The use of LIDAR data helped provide otherwise unavailable topographic data that was within the reservoir footprint but above the water surface elevation while conducting the hydrographic survey. However, there remained some areas approximately between elevations 207.0 feet and 212.0 feet for which no data could be obtained, primarily in shallow areas along the periphery of the lake that were inaccessible by boat or too shallow for the instruments to work properly. The TIN models developed in this range of elevations led to the creation of anomalous "flat triangles", that is triangles whose three vertices all have the same elevation. The flat triangles in turn lead to anomalous calculations of surface area and volume in these elevation ranges. To eliminate the effects of the flat triangles on area and volume calculations, areas between elevations 207.0 feet and 212.0 feet were
linearly interpolated between the computed values, and volumes above elevation 207.0 feet were recalculated based on the corrected areas. The elevation-capacity table and elevationarea table, updated for 2012, are presented in Appendices A and B, respectively. The areacapacity curves are presented in Appendix C.

The volumetric TIN model was converted to a raster representation using a cell size of 2 feet by 2 feet. The raster data was then used to produce an elevation relief map (Figure 4), representing the topography of the reservoir bottom; a depth range map (Figure 5), showing shaded depth ranges for Choke Canyon Reservoir; and a 5-foot contour map (Figure 6 - attached).

Figure 4

## Choke Canyon Reservoir



Figure 5

## Choke Canyon Reservoir



## Analysis of sediment data from Choke Canyon Reservoir

Sedimentation in Choke Canyon Reservoir was determined by analyzing the acoustic signal returns of all three depth sounder frequencies in the DepthPic© software. The 200 kHz signal was analyzed to determine the current bathymetric surface of the reservoir, while all three frequencies, $200 \mathrm{kHz}, 50 \mathrm{kHz}$, and 24 kHz , were analyzed to determine the reservoir bathymetric surface at the time of initial impoundment (i.e. preimpoundment surface). Sediment core samples collected in the reservoir were used to assist in identifying the location of the pre-impoundment surface in the acoustic signals. The difference between the current surface and the pre-impoundment surface yields a sediment thickness value at each sounding location.

Analysis of the sediment core samples was conducted at TWDB headquarters in Austin. Each sample was split longitudinally and analyzed to identify the location of the pre-impoundment surface. The pre-impoundment surface is identified within the sediment core sample by one or both of the following methods: (1) a visual examination of the sediment core for organic materials, such as leaf litter, tree bark, twigs, intact roots, etc., concentrations of which tend to occur on or just below the pre-impoundment surface; (2) changes in texture from well sorted, relatively fine-grained sediment to poorly sorted mixtures of coarse and fine-grained materials; and (3) variations in the physical properties of the sediment, particularly sediment water content and penetration resistance with depth (Van Metre et al., 2004). The total sample length, sediment thickness, and the preimpoundment thickness were recorded. Physical characteristics of the sediment core, including color, texture, relative water content, and presence of organic materials, were also recorded (Table 2).

Table 2. Sediment core sampling analysis data - Choke Canyon Reservoir

| Core | Easting ${ }^{\text {a }}$ <br> (ft) | Northing ${ }^{\text {a }}$ <br> (ft) | Total core sample/ postimpoundment sediment | Sediment core description | Munsell soil color |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C-1 | 2208882.14 | 13362009.91 | 22.5"/13" | $0-1.5 "$ muddy water/ very loose, suspended sediment | N/A |
|  |  |  |  | 1.5-7" high water content, silty with some fine sand | 10YR 3/2 |
|  |  |  |  | 7-8.5" high water content, clay loam | 5Y 2.5/1 |
|  |  |  |  | 8.5-13" high water content, silty with some fine sand | 10YR 3/2 |
|  |  |  |  | 13-22.5" lower water content, higher density soil with peds present, organics present | 5Y 2.5/2 |
| C-2 | 2205251.33 | 13365536.06 | 28"/18" | $0-18 "$ muddy water/ loose suspended sediment | N/A |
|  |  |  |  | 18-28" high water content, silty soil, some roots/ organics present | $2.5 \mathrm{Y} 4 / 2$ |
| C-3 | 2199221.75 | 13357528.51 | 28.5"/17.5" | $0-0.5$ " muddy water/suspended sediment | N/A |
|  |  |  |  | 0.5-17.5" high water content, silty clay sediment | 10YR 3/2 |
|  |  |  |  | 17.5-28.5" lower water content, higher density soil with peds present, roots and organics present | 2.5Y 2.5/2 |
| C-4 | 2191533.74 | 13366153.01 | $25.5 " / 10 "$ | $0-10$ " high water content, silty clay sediment | 10YR 3/1 |
|  |  |  |  | 10-25.5" lower water content, higher density soil, organics present | 5Y 2.5/2 |
| C-5 | 2182914.44 | 13371974.17 | 27"/19" | 0-1" Muddy water/suspended sediment | N/A |
|  |  |  |  | 1-19" high water content, silty clay sediment | 10YR 3/1 |
|  |  |  |  | 19-27" lower water content, clay soil, organics present | 2.5Y 2.5/1 |
| C-6 | 2177447.27 | 13371375.51 | 19"/11" | 0-1" muddy water/ suspended sediment | N/A |
|  |  |  |  | 1-8" high water content, silty sediment | 10YR 3/2 |
|  |  |  |  | 8-9.5" high water content, clay sediment with some organics | 5Y 2.5/1 |
|  |  |  |  | 9.5-11" high water content, silty sediment | 10YR 3/2 |
|  |  |  |  | 11-19" lower water content, clay soil with peds present, roots and organics present | 5Y 2.5/2 |
| C-7 | 2173969.18 | 13363486.84 | $9.5 " / 5.5 "$ | $0-5.5 "$ high water content, silty sediment | 10YR 3/2 |
|  |  |  |  | 5.5-9.5" lower water content, dense clay soil with peds present, organics present | 5Y 2.5/1 |
| C-8 | 2174348.78 | 13357927.85 | $35.5 " / 27.5$ " | 0-3" lost out top when cutting to length | N/A |
|  |  |  |  | 3-27.5" high water content, silty sediment | 10YR 3/1 |
|  |  |  |  | 27.5-35.5" lower water content, dense clay soil with peds, organics and roots present | 5Y 2.5/2 |

[^0]A photograph of sediment core C-8 is shown in Figure 7 and is representative of the sediment cores sampled from Choke Canyon Reservoir. The 200 kHz frequency measures the top layer as the current bottom surface of the reservoir.


Figure 3. Sediment core C-8 from Choke Canyon Reservoir
Sediment core sample C-8 consisted of 35.5 inches of total sediment. The upper sediment layer (horizon), $0-3.0$ inches, was lost when the core tube was cut to length (in Figure 7, the tape measure was extended three inches to compensate for the lost sediment when the core tube was cut too short). The second horizon, beginning at 3.0 inches and extending to 27.5 inches below the surface, consisted of a silty sediment with a high water content and 10YR 3/1 Munsell soil color. The third horizon, from 27.5 inches to 35.5 inches consisted of a dense clay soil with peds, organics, and roots present, a lower water content, and 5Y 2.5/2 Munsell soil color. The base of the sample is denoted by the blue line in Figure 7.

The pre-impoundment boundary (yellow line in Figure 7) was evident within this sediment core sample at 27.5 inches and identified by the change in soil color, texture, moisture, porosity, and structure. Identification of the pre-impoundment surface for the remaining sediment cores followed a similar procedure.

Figures 8 and 9 illustrate how measurements from sediment core samples are used with sonar data to help identify the interface between the post- and pre-impoundment layers in the acoustic signal. Within DepthPic©, the current surface is automatically determined based on signal returns from the 200 kHz transducer and verified by TWDB staff, while the pre-impoundment surface must be determined visually. The pre-impoundment surface is first identified along cross-sections for which sediment core samples have been collected.


Figure 4. Comparison of sediment core C-8 with acoustic signal returns
A,E) combined acoustic signal returns, B,F) 200 kHz frequency, $C, G) 50 \mathrm{kHz}$ frequency, D,H) $24 \mathbf{k H z}$ frequency

Figure 8 compares sediment core sample $\mathrm{C}-8$ with the acoustic signals for all frequencies combined (A, E), $200 \mathrm{kHz}(\mathrm{B}, \mathrm{F}), 50 \mathrm{kHz}(\mathrm{C}, \mathrm{G})$, and $24 \mathrm{kHz}(\mathrm{D}, \mathrm{H})$. The sediment core sample is represented in each figure as colored boxes. The yellow boxes represent post-impoundment sediment, and the blue box represents the pre-impoundment sediment. In Figure 8A-D, the bathymetric surfaces are not shown. In Figure 8E, the current bathymetric surface is represented as the top black line and in Figures 8 F-H as the top red line. The pre-impoundment surface is identified by comparing boundaries observed in the $200 \mathrm{kHz}, 50 \mathrm{kHz}$, and 24 kHz signals to the location of the pre-impoundment surface of the sediment core sample. Each sediment core sample was compared to all three frequencies and the boundary in the 200 kHz signal most closely matched the pre-impoundment interface of the sediment core samples; therefore, the 200 kHz signal was used to locate the pre-impoundment layer. The pre-impoundment surface was manually drawn and is represented by the bottom black line in Figure 8E, and by the yellow line in Figures 8F-H.

Figure 9 shows sediment core sample C-8 correlated with the 200 kHz frequency of the nearest surveyed cross-section. The pre-impoundment surface identified along crosssections where sediment core samples were collected is used as a guide for identifying the pre-impoundment surface along cross-sections where sediment core samples were not collected.


Figure 5. Cross-section of data collected during 2012 survey, displayed in DepthPic© ( 200 kHz frequency), correlated with sediment core sample C-8 and showing the current surface in red and pre-impoundment surface in yellow

After the pre-impoundment surface from all cross-sections was identified, a sediment thickness TIN model is created following standard GIS techniques (Furnans, 2007). Sediment thicknesses were interpolated between surveyed cross-sections using HydroTools with the same interpolation definition file used for bathymetric interpolation. For the purposes of the TIN model creation, TWDB assumed sediment thickness at the reservoir boundary and contours was zero feet (defined as the 220.5 foot NGVD29, 216.78 foot, and 207.98 foot elevation contours). The sediment thickness TIN model was converted to a raster representation using a cell size of 5 feet by 5 feet and used to produce a sediment thickness map of Choke Canyon Reservoir (Figure 10).

Figure 10


## Survey results

## Volumetric survey

The results of the 2012 TWDB volumetric survey indicate Choke Canyon Reservoir has a total reservoir capacity of $\mathbf{6 6 2 , 8 2 1}$ acre-feet and encompasses $\mathbf{2 5 , 4 3 8}$ acres at conservation pool elevation (220.5 feet NGVD29). The original design estimate indicates Choke Canyon Reservoir had a total capacity of 691,130 acre-feet and encompassed 25,733 acres at the time of impoundment in 1982. An area-capacity table provided to TWBD by the U.S. Bureau of Reclamation dated 1983 indicates Choke Canyon Reservoir had a total reservoir capacity of 695,125 acre-feet and encompassed 25,989 acres. A previous survey of Choke Canyon Reservoir by TWDB in 1993 indicated Choke Canyon Reservoir had a total capacity of 695,271 acre-feet and encompassed 25,989 acres. Because of differences in past and present survey methodologies, direct comparison of volumetric surveys to estimate loss of capacity is difficult and can be unreliable.

## Table 3. Current and previous survey capacity and surface area data

| Survey* | Surface area <br> (acres) | Total capacity <br> (acre-feet) |
| :---: | :---: | :---: |
| ${\text { Original, } 1982^{\text {a }}}^{25,733}$ | 691,130 |  |
| USBR $1983^{\text {b }}$ | 25,989 | 695,125 |
| TWDB 1993 | 25,989 | 695,271 |
| TWDB 2012 | 25,438 | 662,821 |

${ }^{\text {a }}$ Source: (TWDB, 2003)
${ }^{\mathrm{b}}$ Source: (WDFT, 2013)

## Sedimentation survey

Based on two methods for estimating sedimentation rates, the 2012 TWDB sedimentation survey estimates Choke Canyon Reservoir loses between 944 and 1,708 acre-feet per year of capacity below conservation pool elevation ( 220.5 feet above mean sea level, NGVD29) due to sedimentation (Table 4). The sedimentation survey indicates sediment accumulation is somewhat consistent throughout the reservoir. The heaviest accumulations measured by this survey are within the submerged river channels. Accumulation in the Frio River channel becomes heavier as it approaches the dam. Comparison of capacity estimates of Choke Canyon Reservoir derived using differing methodologies are provided in Table 4 for sedimentation rate calculation.

Table 4.
Capacity loss comparisons for Choke Canyon Reservoir

| Survey | Volume comparisons at conservation pool elevation, 220.5 feet (acre-feet) |  |  |  | Volume comparison at elevation 207.98 feet (acre-feet) |  | Pre-impoundment below elevation 207.98 feet |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Original 1982 ${ }^{\text {a }}$ | 691,130 | <> | <> | <> | <> | $\stackrel{ }{<}$ | <> |
| USBR $1983{ }^{\text {b }}$ | <> | 695,125 | <> | <> | 413,291 | <> | <> |
| TWDB 1993 | <> | <> | 695,271 | <> | <> | $413,365{ }^{\text {d }}$ | <> |
| TWDB preimpoundment estimate based on 2012 survey | <> | <> | <> | 696,239 ${ }^{\text {c }}$ | <> | < | 414,405 ${ }^{\text {e }}$ |
| 2012 volumetric survey | 662,821 | 662,821 | 662,821 | 662,821 | 388,395 | 388,395 | 388,395 |
| Volume difference (acre-feet) | 28,309 (4.1\%) | 32,304 (4.6\%) | 32,450 (4.7\%) | 33,418 (4.8\%) | 24,896 (6.0\%) | 24,970 (6.0\%) | 26,010 (6.3\%) |
| Number of years | 30 | 29 | 19 | 30 | 29 | 19 | 30 |
| Capacity loss rate (acre-feet/year) | 944 | 1,114 | 1,708 | 1,114 | 830 | 1,314 | 867 |

${ }^{\text {a }}$ Source: (TWDB, 2003), note: Choke Canyon Dam was completed in 1982
${ }^{\mathrm{b}}$ Source: (WDFT, 2013)
${ }^{\text {c }} 2012$ TWDB surveyed capacity of 662,821 acre-feet plus 2012 TWDB surveyed sediment volume of 26,010 acre-feet at elevation 207.98 feet and the calculated volume difference from the 1983 and 2012 surveys between elevations 207.98 feet and 220.5 feet of 7,408 acre-feet
${ }^{\text {d }}$ Derived using linear interpolation of values at 207.9 and 208.0 feet from 1993 TWDB capacity table
${ }^{\text {e }} 2012$ TWDB surveyed capacity of 388,395 acre-feet plus 2012 TWDB surveyed sediment volume of 26,010 acre-feet at elevation 207.98 feet

## Recommendations

To improve estimates of sediment accumulation rates, TWDB recommends resurveying Choke Canyon Reservoir in approximately 10 years or after a major flood event. To further improve estimates of sediment accumulation, TWDB recommends another sedimentation survey. A resurvey would allow a more accurate quantification of the average sediment accumulation rate for Choke Canyon Reservoir.

## TWDB contact information

More information about the Hydrographic Survey Program can be found at:
http://www.twdb.texas.gov/surfacewater/surveys/index.asp
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Choke Canyon Reservoir RESERVOIR CAPACITY TABLE

|  | EXAS WATER DEVELOPMENT BOARDCAPACITY IN ACRE-FEET |  |  |  | June 2012 Survey <br> Conservation Pool Elevation 220.5 feet NGVD29 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ELEVATION in Feet | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 135 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 136 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 2 |
| 137 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 4 | 4 |
| 138 | 4 | 5 | 5 | 5 | 6 | 6 | 6 | 7 | 7 | 7 |
| 139 | 8 | 8 | 8 | 9 | 9 | 10 | 10 | 11 | 11 | 12 |
| 140 | 13 | 13 | 14 | 15 | 15 | 16 | 17 | 18 | 19 | 20 |
| 141 | 21 | 22 | 23 | 24 | 26 | 27 | 28 | 30 | 31 | 33 |
| 142 | 35 | 37 | 39 | 41 | 43 | 45 | 47 | 49 | 51 | 54 |
| 143 | 56 | 58 | 61 | 63 | 66 | 68 | 71 | 74 | 77 | 80 |
| 144 | 83 | 86 | 89 | 92 | 95 | 99 | 103 | 106 | 110 | 114 |
| 145 | 118 | 122 | 126 | 131 | 135 | 140 | 144 | 149 | 154 | 159 |
| 146 | 165 | 170 | 176 | 181 | 187 | 193 | 199 | 205 | 211 | 217 |
| 147 | 223 | 229 | 236 | 242 | 249 | 256 | 263 | 270 | 277 | 284 |
| 148 | 292 | 299 | 307 | 315 | 323 | 331 | 339 | 347 | 355 | 364 |
| 149 | 372 | 381 | 390 | 399 | 408 | 417 | 427 | 436 | 446 | 456 |
| 150 | 467 | 477 | 488 | 498 | 509 | 521 | 533 | 545 | 557 | 570 |
| 151 | 584 | 598 | 612 | 626 | 641 | 656 | 672 | 687 | 703 | 720 |
| 152 | 737 | 754 | 771 | 789 | 807 | 825 | 844 | 863 | 883 | 903 |
| 153 | 923 | 944 | 965 | 986 | 1,008 | 1,030 | 1,053 | 1,076 | 1,099 | 1,122 |
| 154 | 1,146 | 1,171 | 1,196 | 1,221 | 1,247 | 1,273 | 1,299 | 1,326 | 1,353 | 1,381 |
| 155 | 1,409 | 1,438 | 1,467 | 1,496 | 1,526 | 1,557 | 1,588 | 1,619 | 1,651 | 1,683 |
| 156 | 1,716 | 1,750 | 1,784 | 1,818 | 1,853 | 1,889 | 1,925 | 1,961 | 1,998 | 2,036 |
| 157 | 2,074 | 2,113 | 2,152 | 2,192 | 2,233 | 2,274 | 2,316 | 2,358 | 2,401 | 2,445 |
| 158 | 2,490 | 2,535 | 2,580 | 2,627 | 2,674 | 2,722 | 2,771 | 2,821 | 2,871 | 2,922 |
| 159 | 2,974 | 3,026 | 3,080 | 3,134 | 3,188 | 3,244 | 3,301 | 3,358 | 3,416 | 3,475 |
| 160 | 3,535 | 3,596 | 3,658 | 3,722 | 3,786 | 3,852 | 3,919 | 3,987 | 4,056 | 4,127 |
| 161 | 4,199 | 4,272 | 4,346 | 4,421 | 4,497 | 4,575 | 4,654 | 4,734 | 4,815 | 4,897 |
| 162 | 4,980 | 5,065 | 5,152 | 5,239 | 5,328 | 5,418 | 5,509 | 5,602 | 5,696 | 5,791 |
| 163 | 5,888 | 5,986 | 6,086 | 6,187 | 6,290 | 6,394 | 6,500 | 6,608 | 6,718 | 6,830 |
| 164 | 6,944 | 7,060 | 7,178 | 7,298 | 7,420 | 7,544 | 7,670 | 7,798 | 7,927 | 8,058 |
| 165 | 8,191 | 8,326 | 8,463 | 8,602 | 8,743 | 8,886 | 9,031 | 9,177 | 9,325 | 9,474 |
| 166 | 9,625 | 9,778 | 9,932 | 10,088 | 10,245 | 10,404 | 10,565 | 10,728 | 10,892 | 11,058 |
| 167 | 11,226 | 11,396 | 11,567 | 11,741 | 11,917 | 12,094 | 12,274 | 12,455 | 12,639 | 12,824 |
| 168 | 13,011 | 13,200 | 13,391 | 13,584 | 13,780 | 13,978 | 14,178 | 14,380 | 14,586 | 14,795 |
| 169 | 15,007 | 15,222 | 15,439 | 15,658 | 15,880 | 16,105 | 16,331 | 16,561 | 16,794 | 17,029 |
| 170 | 17,267 | 17,508 | 17,751 | 17,997 | 18,245 | 18,497 | 18,752 | 19,009 | 19,270 | 19,533 |
| 171 | 19,799 | 20,068 | 20,340 | 20,614 | 20,892 | 21,174 | 21,458 | 21,746 | 22,038 | 22,332 |
| 172 | 22,629 | 22,929 | 23,231 | 23,537 | 23,845 | 24,157 | 24,471 | 24,788 | 25,109 | 25,432 |
| 173 | 25,758 | 26,087 | 26,420 | 26,756 | 27,095 | 27,438 | 27,785 | 28,134 | 28,487 | 28,844 |
| 174 | 29,203 | 29,565 | 29,931 | 30,300 | 30,671 | 31,046 | 31,424 | 31,805 | 32,190 | 32,578 |
| 175 | 32,968 | 33,362 | 33,760 | 34,160 | 34,564 | 34,971 | 35,381 | 35,794 | 36,211 | 36,630 |
| 176 | 37,053 | 37,479 | 37,907 | 38,339 | 38,773 | 39,209 | 39,649 | 40,091 | 40,536 | 40,984 |
| 177 | 41,435 | 41,889 | 42,347 | 42,808 | 43,271 | 43,739 | 44,210 | 44,685 | 45,164 | 45,647 |
| 178 | 46,134 | 46,625 | 47,119 | 47,619 | 48,123 | 48,632 | 49,145 | 49,662 | 50,182 | 50,707 |
| 179 | 51,236 | 51,769 | 52,306 | 52,847 | 53,392 | 53,942 | 54,495 | 55,053 | 55,615 | 56,181 |
| 180 | 56,751 | 57,326 | 57,905 | 58,487 | 59,074 | 59,665 | 60,260 | 60,859 | 61,462 | 62,069 |
| 181 | 62,680 | 63,295 | 63,915 | 64,538 | 65,165 | 65,796 | 66,432 | 67,071 | 67,715 | 68,363 |
| 182 | 69,015 | 69,671 | 70,332 | 70,998 | 71,668 | 72,342 | 73,021 | 73,703 | 74,390 | 75,080 |
| 183 | 75,774 | 76,472 | 77,175 | 77,881 | 78,591 | 79,305 | 80,024 | 80,746 | 81,472 | 82,202 |
| 184 | 82,936 | 83,674 | 84,416 | 85,163 | 85,915 | 86,671 | 87,431 | 88,196 | 88,966 | 89,740 |
| 185 | 90,518 | 91,301 | 92,089 | 92,881 | 93,677 | 94,479 | 95,284 | 96,095 | 96,909 | 97,728 |
| 186 | 98,551 | 99,379 | 100,212 | 101,049 | 101,891 | 102,737 | 103,588 | 104,443 | 105,302 | 106,165 |
| 187 | 107,033 | 107,905 | 108,781 | 109,661 | 110,545 | 111,432 | 112,324 | 113,220 | 114,119 | 115,023 |
| 188 | 115,931 | 116,842 | 117,758 | 118,678 | 119,602 | 120,531 | 121,463 | 122,400 | 123,341 | 124,285 |
| 189 | 125,234 | 126,186 | 127,143 | 128,104 | 129,069 | 130,038 | 131,012 | 131,990 | 132,972 | 133,958 |

## Appendix A (Continued)

## Choke Canyon Reservoir RESERVOIR CAPACITY TABLE



[^1]
## Appendix B

## Choke Canyon Reservoir RESERVOIR AREA TABLE

| TEXAS WATER DEVELOPMENT BOARD AREA IN ACRES |  |  |  |  | June 2012 Survey <br> Conservation Pool Elevation 220.5 feet NGVD29 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |
| ELEVATION in Feet | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 135 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 136 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 137 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 |
| 138 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 4 | 4 |
| 139 | 4 | 4 | 4 | 4 | 5 | 5 | 5 | 6 | 6 | 6 |
| 140 | 6 | 7 | 7 | 7 | 8 | 8 | 9 | 9 | 10 | 10 |
| 141 | 11 | 11 | 11 | 12 | 12 | 13 | 14 | 17 | 17 | 18 |
| 142 | 18 | 19 | 20 | 20 | 21 | 21 | 22 | 22 | 23 | 23 |
| 143 | 23 | 24 | 24 | 25 | 26 | 26 | 27 | 28 | 28 | 29 |
| 144 | 30 | 31 | 32 | 33 | 34 | 36 | 37 | 38 | 39 | 40 |
| 145 | 41 | 42 | 43 | 44 | 45 | 47 | 48 | 49 | 51 | 52 |
| 146 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 |
| 147 | 63 | 64 | 65 | 66 | 67 | 69 | 70 | 71 | 72 | 73 |
| 148 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 83 | 84 | 85 |
| 149 | 86 | 88 | 89 | 91 | 92 | 94 | 96 | 98 | 99 | 101 |
| 150 | 103 | 105 | 107 | 109 | 112 | 116 | 120 | 124 | 128 | 132 |
| 151 | 136 | 140 | 143 | 146 | 149 | 153 | 156 | 159 | 163 | 166 |
| 152 | 169 | 173 | 176 | 179 | 183 | 186 | 190 | 194 | 198 | 201 |
| 153 | 205 | 208 | 212 | 216 | 219 | 223 | 227 | 231 | 235 | 238 |
| 154 | 243 | 247 | 251 | 255 | 259 | 263 | 267 | 271 | 275 | 280 |
| 155 | 284 | 288 | 293 | 297 | 302 | 306 | 311 | 316 | 321 | 327 |
| 156 | 332 | 337 | 342 | 347 | 352 | 358 | 363 | 368 | 373 | 379 |
| 157 | 384 | 390 | 396 | 402 | 409 | 415 | 421 | 428 | 435 | 442 |
| 158 | 448 | 455 | 462 | 469 | 476 | 484 | 491 | 499 | 507 | 515 |
| 159 | 522 | 529 | 537 | 544 | 552 | 560 | 568 | 577 | 586 | 596 |
| 160 | 606 | 617 | 627 | 639 | 651 | 663 | 675 | 687 | 699 | 712 |
| 161 | 724 | 736 | 747 | 758 | 769 | 781 | 793 | 805 | 817 | 829 |
| 162 | 842 | 856 | 868 | 880 | 893 | 906 | 920 | 934 | 948 | 962 |
| 163 | 976 | 990 | 1,004 | 1,020 | 1,036 | 1,052 | 1,068 | 1,088 | 1,107 | 1,129 |
| 164 | 1,152 | 1,172 | 1,191 | 1,210 | 1,229 | 1,249 | 1,268 | 1,286 | 1,303 | 1,321 |
| 165 | 1,341 | 1,361 | 1,380 | 1,399 | 1,419 | 1,437 | 1,455 | 1,471 | 1,486 | 1,501 |
| 166 | 1,517 | 1,533 | 1,550 | 1,566 | 1,583 | 1,599 | 1,617 | 1,634 | 1,652 | 1,670 |
| 167 | 1,689 | 1,708 | 1,727 | 1,746 | 1,766 | 1,786 | 1,805 | 1,824 | 1,843 | 1,863 |
| 168 | 1,881 | 1,901 | 1,921 | 1,944 | 1,966 | 1,988 | 2,012 | 2,041 | 2,076 | 2,106 |
| 169 | 2,132 | 2,159 | 2,184 | 2,207 | 2,231 | 2,255 | 2,282 | 2,310 | 2,339 | 2,367 |
| 170 | 2,395 | 2,419 | 2,445 | 2,473 | 2,502 | 2,532 | 2,559 | 2,589 | 2,618 | 2,647 |
| 171 | 2,676 | 2,703 | 2,731 | 2,763 | 2,797 | 2,831 | 2,864 | 2,896 | 2,927 | 2,955 |
| 172 | 2,984 | 3,012 | 3,040 | 3,069 | 3,099 | 3,130 | 3,160 | 3,188 | 3,217 | 3,247 |
| 173 | 3,278 | 3,309 | 3,343 | 3,377 | 3,412 | 3,446 | 3,478 | 3,514 | 3,548 | 3,579 |
| 174 | 3,609 | 3,640 | 3,671 | 3,702 | 3,733 | 3,763 | 3,797 | 3,830 | 3,861 | 3,892 |
| 175 | 3,924 | 3,955 | 3,990 | 4,023 | 4,054 | 4,085 | 4,118 | 4,148 | 4,180 | 4,211 |
| 176 | 4,241 | 4,270 | 4,300 | 4,328 | 4,355 | 4,381 | 4,408 | 4,435 | 4,464 | 4,495 |
| 177 | 4,527 | 4,558 | 4,591 | 4,623 | 4,656 | 4,691 | 4,729 | 4,769 | 4,809 | 4,849 |
| 178 | 4,889 | 4,929 | 4,971 | 5,019 | 5,068 | 5,108 | 5,148 | 5,186 | 5,226 | 5,269 |
| 179 | 5,310 | 5,351 | 5,391 | 5,430 | 5,472 | 5,514 | 5,555 | 5,598 | 5,642 | 5,685 |
| 180 | 5,726 | 5,766 | 5,807 | 5,847 | 5,889 | 5,930 | 5,971 | 6,011 | 6,051 | 6,089 |
| 181 | 6,131 | 6,171 | 6,212 | 6,252 | 6,293 | 6,334 | 6,374 | 6,414 | 6,457 | 6,500 |
| 182 | 6,542 | 6,587 | 6,633 | 6,676 | 6,723 | 6,765 | 6,807 | 6,847 | 6,884 | 6,922 |
| 183 | 6,961 | 7,001 | 7,041 | 7,082 | 7,124 | 7,164 | 7,202 | 7,241 | 7,279 | 7,318 |
| 184 | 7,359 | 7,402 | 7,447 | 7,492 | 7,537 | 7,583 | 7,628 | 7,673 | 7,718 | 7,762 |
| 185 | 7,807 | 7,851 | 7,897 | 7,944 | 7,991 | 8,036 | 8,080 | 8,122 | 8,166 | 8,210 |
| 186 | 8,257 | 8,304 | 8,350 | 8,396 | 8,441 | 8,484 | 8,527 | 8,569 | 8,613 | 8,656 |
| 187 | 8,697 | 8,738 | 8,781 | 8,821 | 8,860 | 8,897 | 8,936 | 8,976 | 9,016 | 9,056 |
| 188 | 9,096 | 9,137 | 9,179 | 9,221 | 9,263 | 9,305 | 9,347 | 9,388 | 9,427 | 9,466 |
| 189 | 9,506 | 9,546 | 9,587 | 9,629 | 9,673 | 9,715 | 9,757 | 9,800 | 9,841 | 9,883 |

Appendix B (Continued)

## Choke Canyon Reservoir

RESERVOIR AREA TABLE

| TEXAS WATER DEVELOPMENT BOARD AREA IN ACRES |  |  |  |  | June 2012 Survey |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Conservation Pool Elevation 220.5 feet NGVD29 |  |  |  |  |  |
| ELEVATION INCREMENT IS ONE TENTH FOOT |  |  |  |  |  |  |  |  |  |  |
| ELEVATION in Feet | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 190 | 9,924 | 9,964 | 10,004 | 10,043 | 10,083 | 10,122 | 10,161 | 10,200 | 10,243 | 10,285 |
| 191 | 10,325 | 10,366 | 10,406 | 10,445 | 10,486 | 10,525 | 10,564 | 10,605 | 10,646 | 10,685 |
| 192 | 10,725 | 10,765 | 10,804 | 10,843 | 10,885 | 10,927 | 10,970 | 11,013 | 11,057 | 11,102 |
| 193 | 11,149 | 11,196 | 11,244 | 11,296 | 11,345 | 11,394 | 11,443 | 11,490 | 11,535 | 11,580 |
| 194 | 11,626 | 11,668 | 11,710 | 11,754 | 11,799 | 11,842 | 11,887 | 11,934 | 11,980 | 12,027 |
| 195 | 12,076 | 12,124 | 12,174 | 12,223 | 12,272 | 12,324 | 12,374 | 12,423 | 12,471 | 12,520 |
| 196 | 12,567 | 12,615 | 12,664 | 12,714 | 12,761 | 12,807 | 12,852 | 12,897 | 12,943 | 12,988 |
| 197 | 13,035 | 13,082 | 13,131 | 13,179 | 13,225 | 13,273 | 13,321 | 13,369 | 13,417 | 13,465 |
| 198 | 13,512 | 13,559 | 13,606 | 13,653 | 13,700 | 13,747 | 13,797 | 13,848 | 13,900 | 13,952 |
| 199 | 14,005 | 14,064 | 14,131 | 14,202 | 14,278 | 14,350 | 14,418 | 14,485 | 14,550 | 14,613 |
| 200 | 14,676 | 14,736 | 14,797 | 14,856 | 14,914 | 14,970 | 15,023 | 15,075 | 15,128 | 15,180 |
| 201 | 15,232 | 15,284 | 15,337 | 15,390 | 15,443 | 15,492 | 15,544 | 15,597 | 15,645 | 15,692 |
| 202 | 15,737 | 15,780 | 15,822 | 15,864 | 15,905 | 15,946 | 15,987 | 16,027 | 16,067 | 16,106 |
| 203 | 16,144 | 16,183 | 16,222 | 16,261 | 16,300 | 16,340 | 16,379 | 16,419 | 16,459 | 16,499 |
| 204 | 16,539 | 16,579 | 16,620 | 16,660 | 16,701 | 16,743 | 16,784 | 16,826 | 16,868 | 16,911 |
| 205 | 16,954 | 16,998 | 17,042 | 17,086 | 17,131 | 17,176 | 17,222 | 17,268 | 17,315 | 17,362 |
| 206 | 17,409 | 17,457 | 17,506 | 17,555 | 17,604 | 17,655 | 17,706 | 17,758 | 17,810 | 17,864 |
| 207 | 17,919 | 17,972 | 18,026 | 18,079 | 18,133 | 18,186 | 18,240 | 18,293 | 18,346 | 18,400 |
| 208 | 18,453 | 18,507 | 18,560 | 18,614 | 18,667 | 18,721 | 18,774 | 18,828 | 18,881 | 18,935 |
| 209 | 18,988 | 19,042 | 19,095 | 19,149 | 19,202 | 19,256 | 19,309 | 19,363 | 19,416 | 19,470 |
| 210 | 19,523 | 19,576 | 19,630 | 19,683 | 19,737 | 19,790 | 19,844 | 19,897 | 19,951 | 20,004 |
| 211 | 20,058 | 20,111 | 20,165 | 20,218 | 20,272 | 20,325 | 20,379 | 20,432 | 20,486 | 20,539 |
| 212 | 20,593 | 20,631 | 20,676 | 20,733 | 20,805 | 20,888 | 20,969 | 21,042 | 21,110 | 21,177 |
| 213 | 21,242 | 21,304 | 21,356 | 21,406 | 21,455 | 21,503 | 21,546 | 21,589 | 21,632 | 21,678 |
| 214 | 21,722 | 21,767 | 21,815 | 21,867 | 21,917 | 21,969 | 22,022 | 22,078 | 22,134 | 22,188 |
| 215 | 22,244 | 22,302 | 22,358 | 22,413 | 22,470 | 22,531 | 22,595 | 22,657 | 22,721 | 22,786 |
| 216 | 22,853 | 22,917 | 22,984 | 23,053 | 23,123 | 23,191 | 23,260 | 23,329 | 23,430 | 23,494 |
| 217 | 23,558 | 23,623 | 23,689 | 23,749 | 23,808 | 23,867 | 23,926 | 23,981 | 24,036 | 24,090 |
| 218 | 24,145 | 24,198 | 24,250 | 24,305 | 24,362 | 24,416 | 24,470 | 24,524 | 24,580 | 24,635 |
| 219 | 24,689 | 24,744 | 24,799 | 24,853 | 24,904 | 24,952 | 25,000 | 25,045 | 25,088 | 25,130 |
| 220 | 25,173 | 25,215 | 25,257 | 25,301 | 25,346 | 25,438 |  |  |  |  |

Note: Values from 207.0 feet to 212.0 feet are linear interpolations between computed values.


Appendix C: Area and Capacity Curves



[^0]:    ${ }^{\text {a }}$ Coordinates are based on NAD83 State Plane Texas South Central System (feet)

[^1]:    Note: Capacities from 207.0 feet to 220.5 feet have been re-calculated based on corrected areas. See Appendix B.

