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DRAFT TECHNICAL MEMORANDUM

Daryn Hardwick, Groundwater Modeling Manager, Texas Water Development Board
Stephanie J. Moore, PG, INTERA Incorporated
April 30, 2025
Final Stakeholder Advisory Forum for Development of the Cross Timbers Aquifer Numerical Model

1 Overview

The second and final Stakeholder Advisory Forum (SAF) for development of the Cross Timbers Aquifer Groundwater Availability Model (GAM) was held on April 16, 2025. The purpose of the SAF was to provide an update on status of model development, share information regarding the current draft numerical model report, and seek public comment on the draft model and report. The agenda included a summary of (1) the Cross Timbers Aquifer Numerical Model, (2) model calibration, (3) sensitivity analysis, (4) model limitations, and (5) discussion.

INTERA, Inc. was retained by the Texas Water Development Board (TWDB) to develop the numerical model for the Cross Timbers Aquifer. INTERA hosted the SAF online via Microsoft Teams. A total of 26 people in attended the meeting. Names and affiliations for each attendee is provided in **Attachment 1**.

Daryn Hardwick of TWDB began the meeting by sharing the location to find all meeting materials for the Cross Timbers Aquifer (<u>https://www.twdb.texas.gov/groundwater/models/gam/cstb/cstb.asp</u>) and an overview of the TWDB Stakeholder Advisory Forums.

Stephanie Moore of INTERA continued with review of the meeting agenda and introduction of the project team. Stephanie Moore, Ryan Harmon, and Savannah Miller of INTERA continued with presentation of the technical details of the study area and numerical model. The complete PowerPoint presentation is provided as **Attachment 2**. An audio and video recording is available at the link listed in the above paragraph.

Upon conclusion of the technical presentations, the project team took questions from the audience. A summary of questions and answers is provided in **Attachment 3**. Finally, Stephanie wrapped up the meeting with reminder that the draft report is currently available for public review through June 16, 2025 (60 days from date of the meeting) and comments should be submitted to gam@twdb.texas.gov.

Attachment 1. Attendees

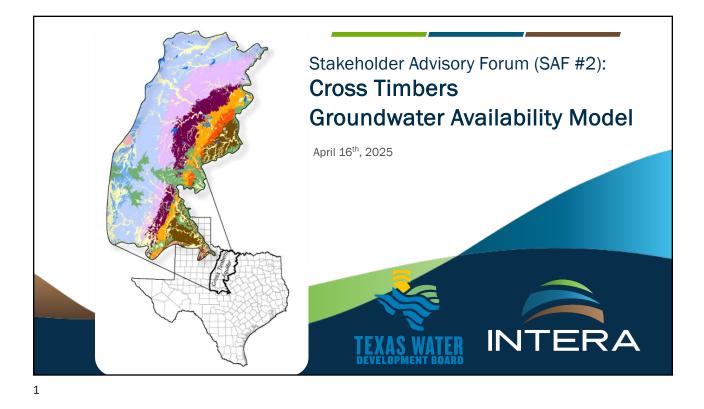
Number	Name	Affiliation
1	Roberto Anaya	TWDB
2	Natalie Ballew	TWDB
3	Neil Blandford	Geo-Logic Associates
4	Robert Bradley	TWDB
5	Ray Brady	Unknown
6	Amy Bush	Consultant
7	Tim Cawthon	TWDB
8	Bence Close	Unknown
9	Neil E. Deeds	INTERA
10	John Ellis	INTERA
11	Jevon Harding	TWDB
12	Daryn Hardwick	TWDB
13	Ryan Harmon	INTERA
14	lan Jones	TWDB
15	Kristie Laughlin	TWDB
16	Adam Lee	TWDB
17	Saheli Majumdar	TWDB
18	Savannah Miller	INTERA
19	Stephanie Moore	INTERA
20	Micaela Pedrazas	TWDB
21	Doug Shaw	Upper Trinity GCD
22	Lynn Smith	Rolling Plains GCD
23	Evan Strickland	TWDB
24	Todd Umstot	Geo-Logic Associates
25	Shirley Wade	TWDB
26	Jeremy White	INTERA



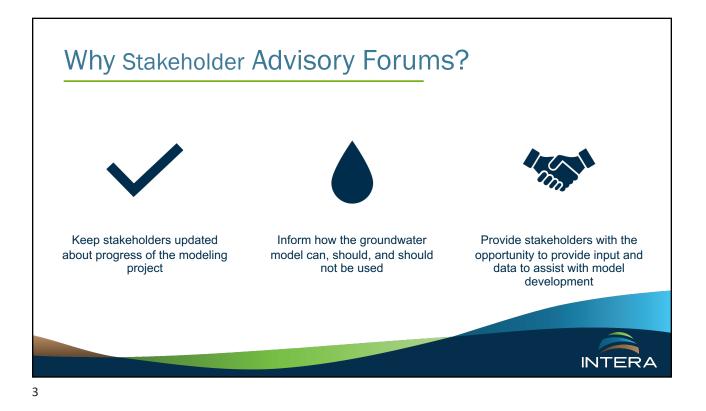
Final Stakeholder Advisory Forum for Development of the Cross Timbers Aquifer Numerical Model April 30, 2025 Page 3

Attachment 2. PowerPoint Slides from SAF#2

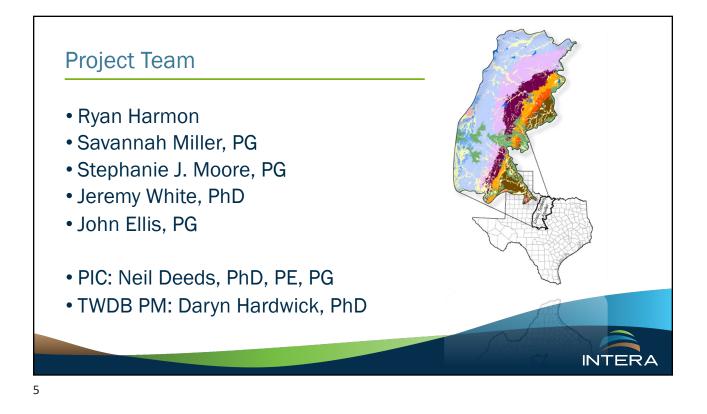


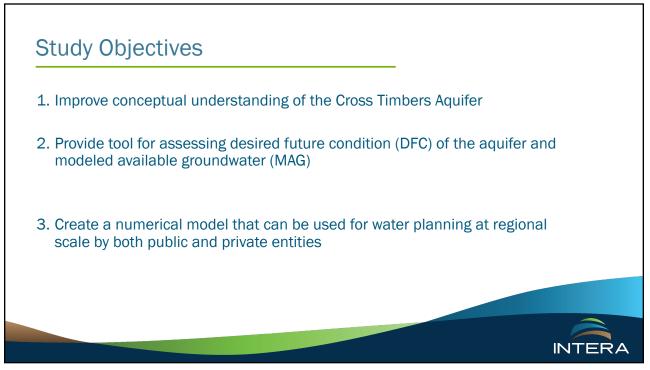


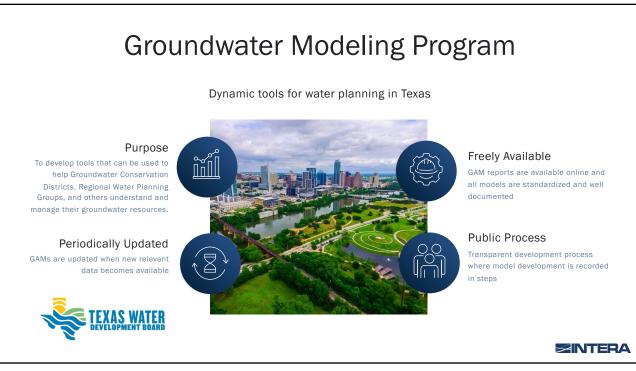




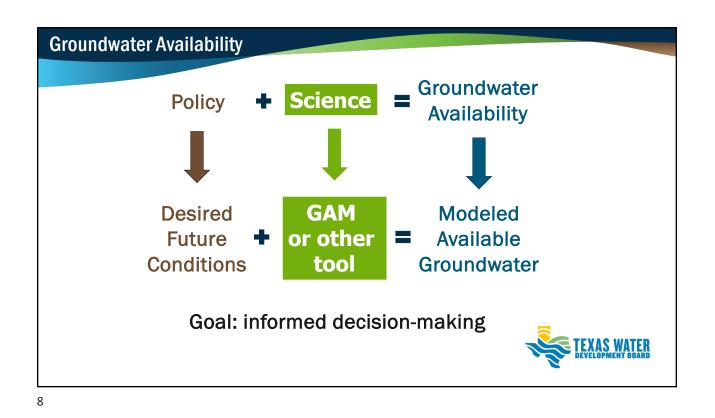


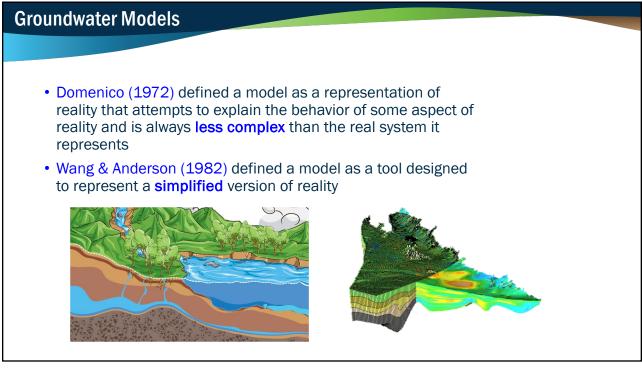




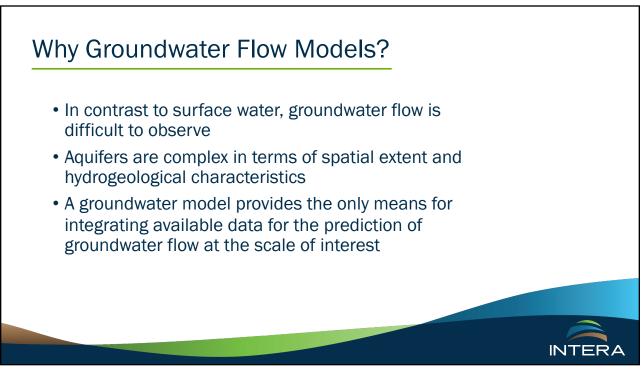


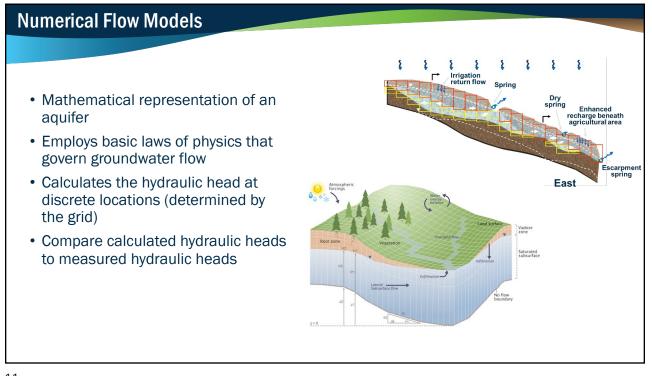


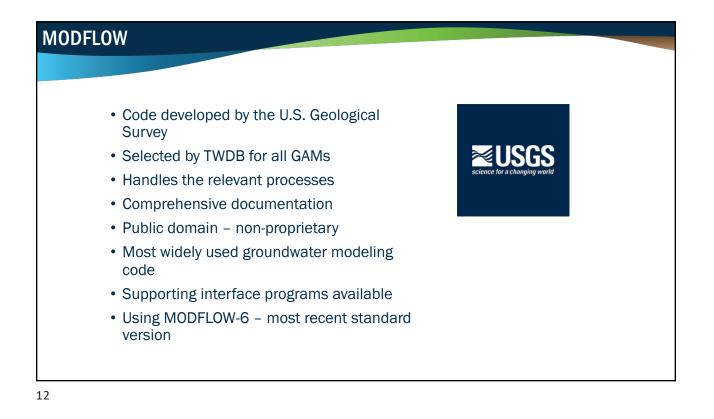


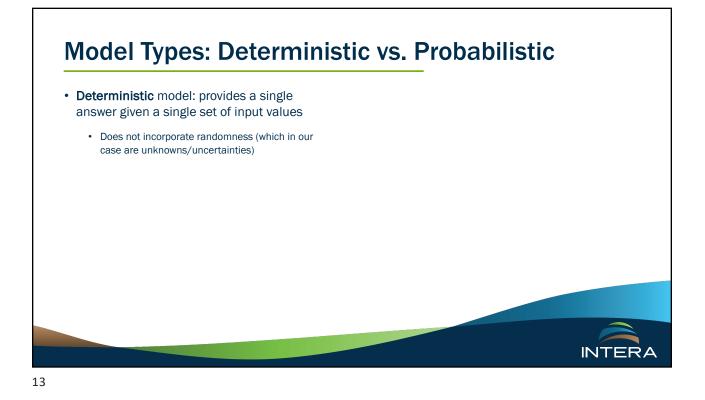


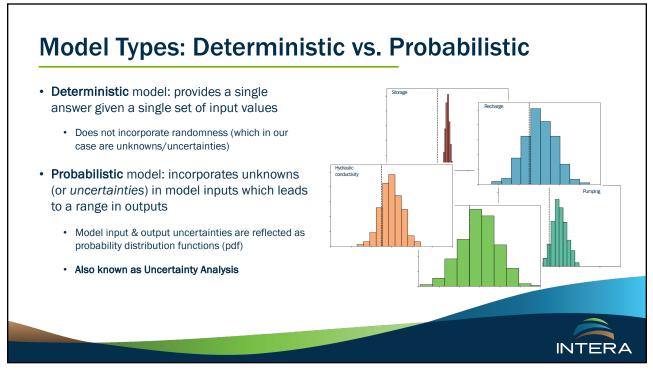


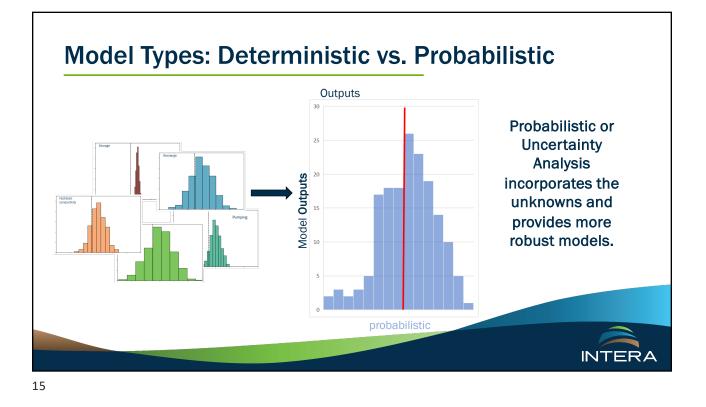


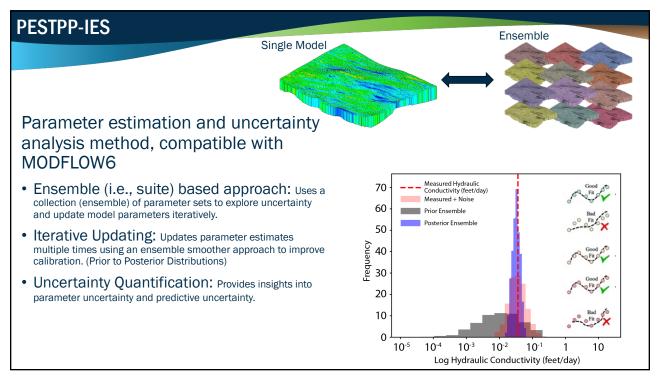


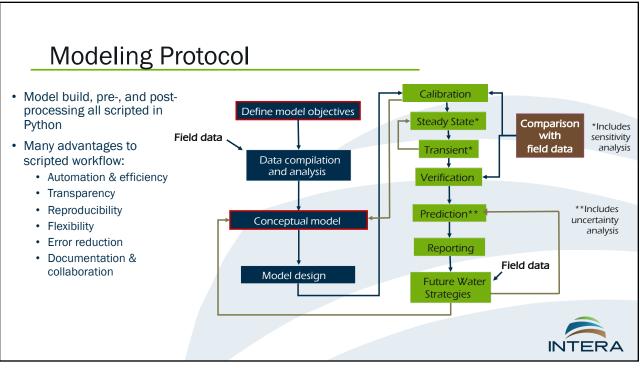


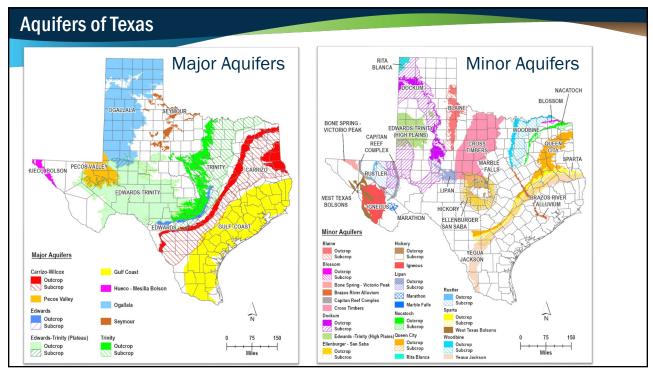


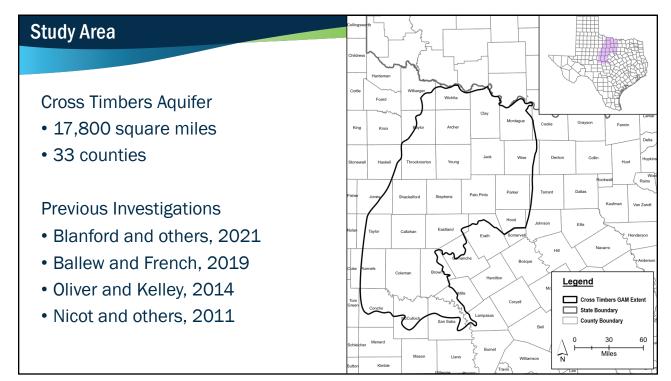


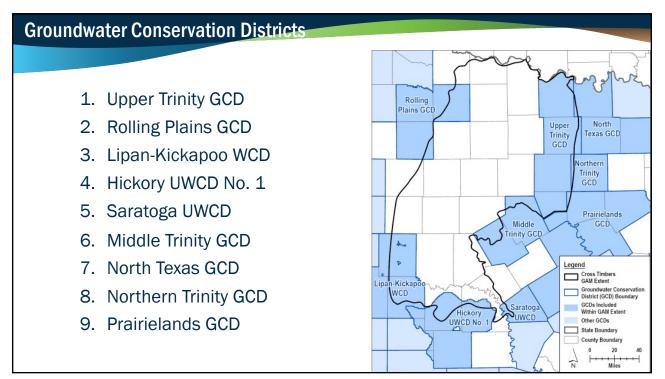


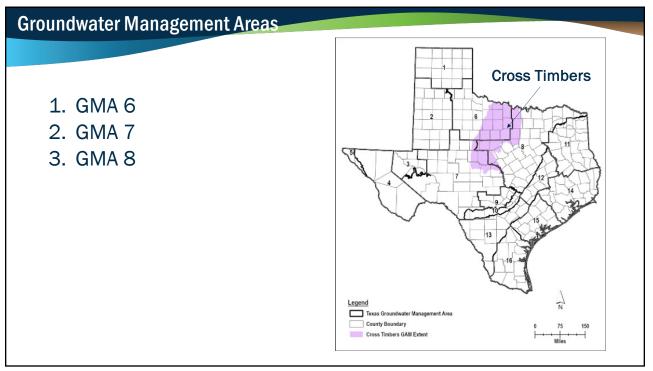


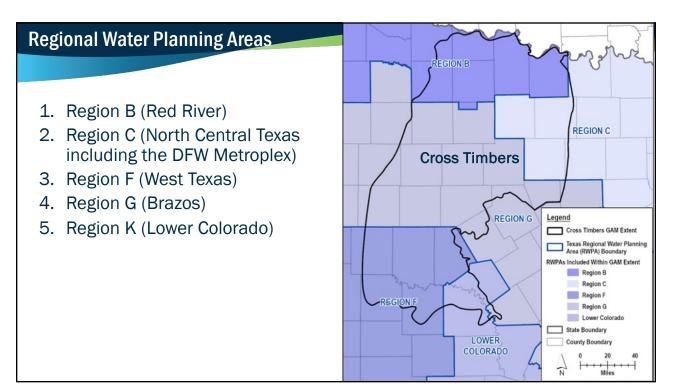


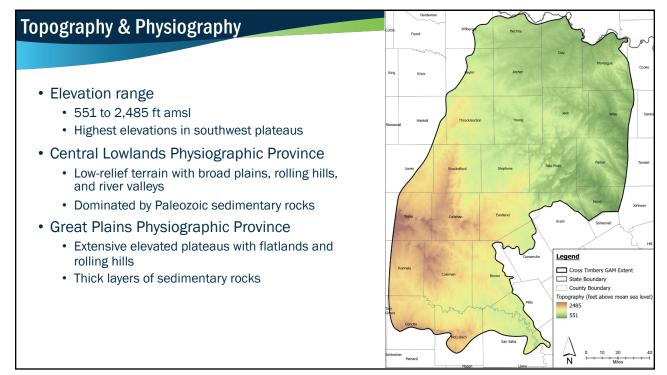


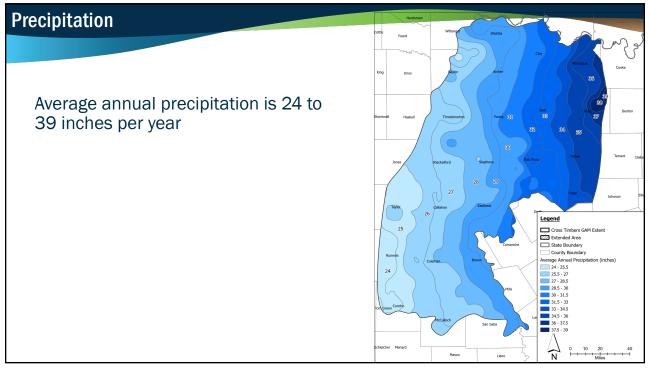


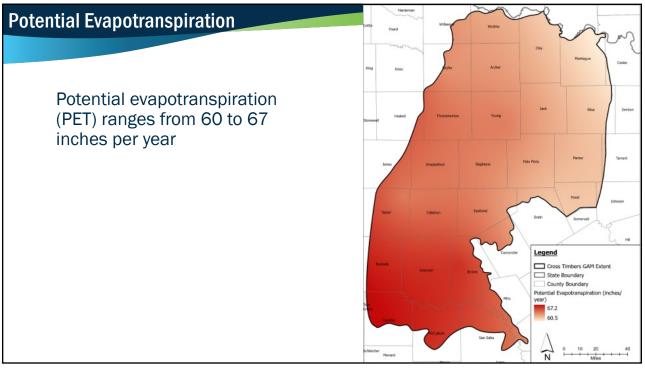


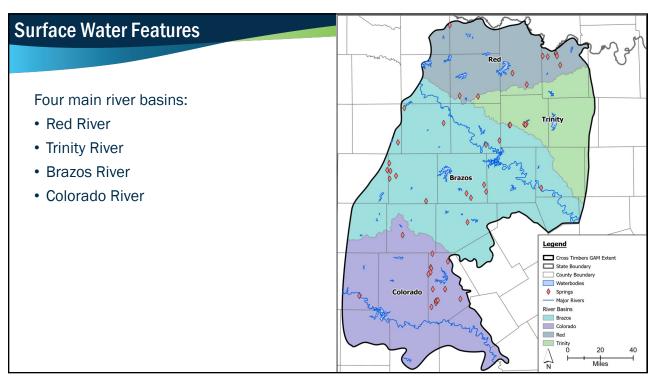


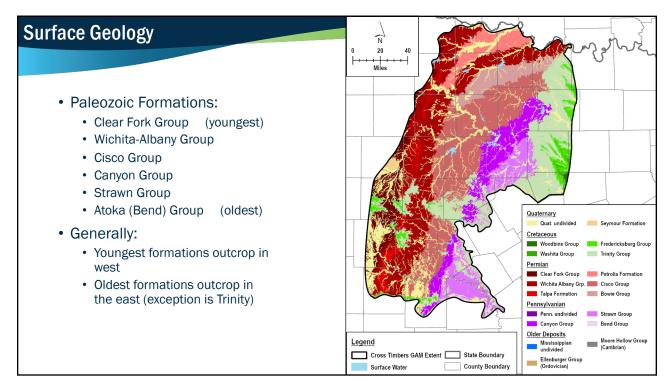


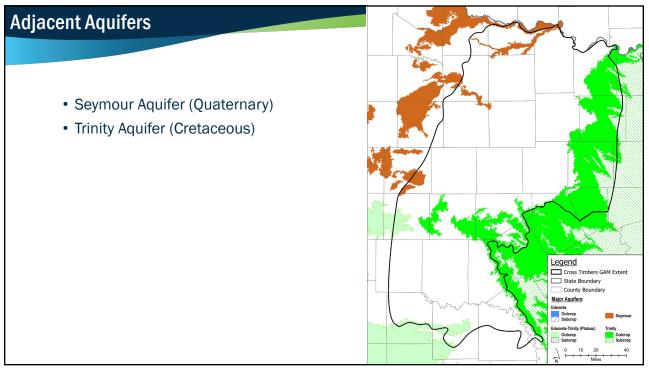


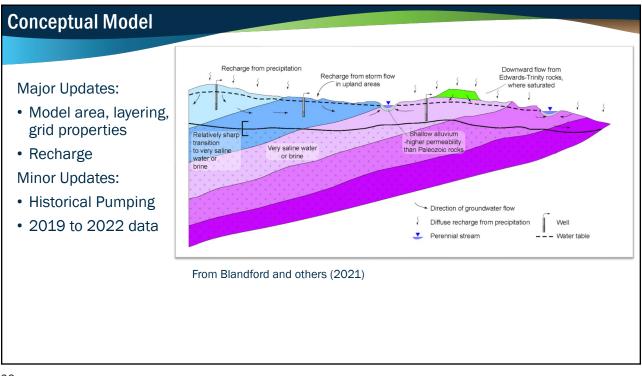


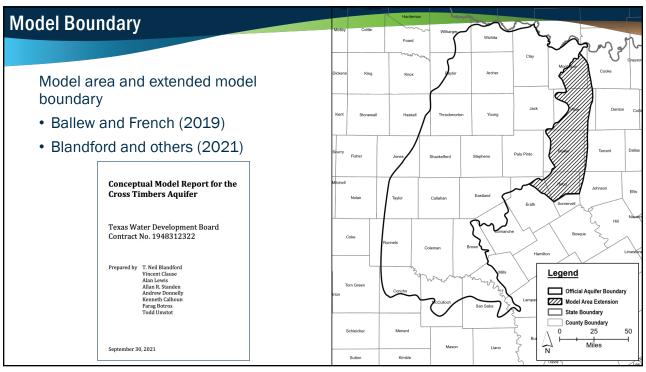


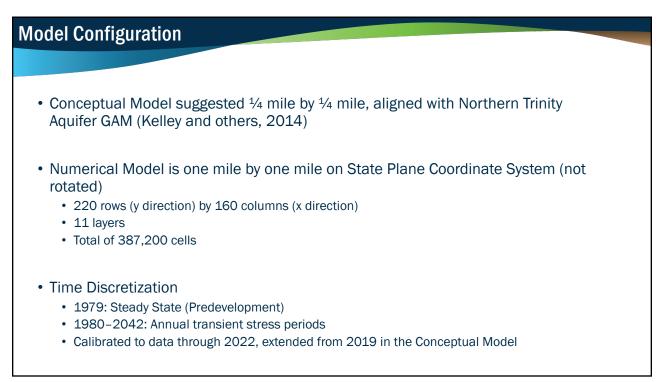




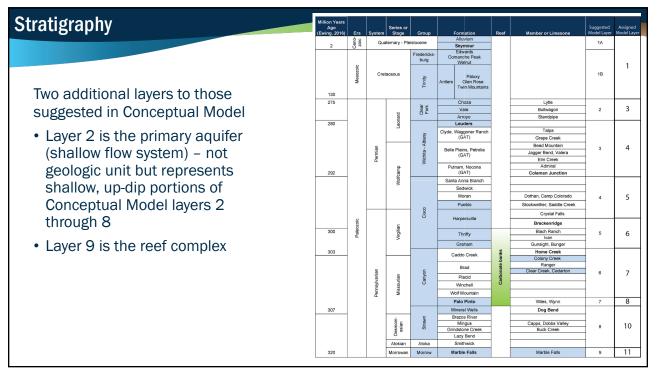




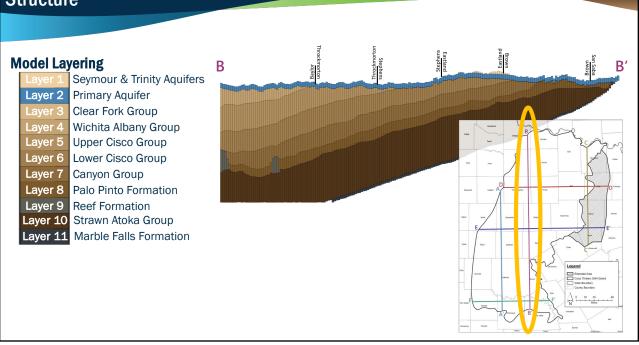


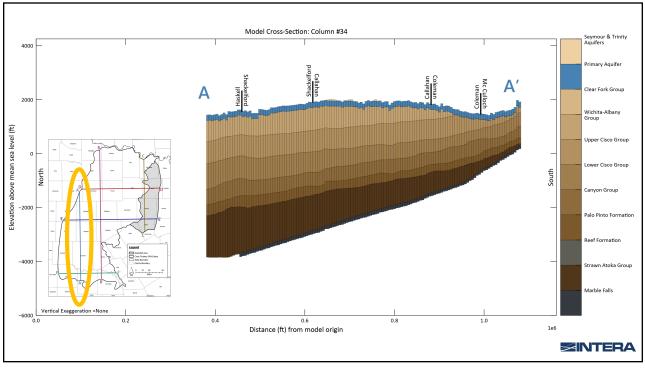


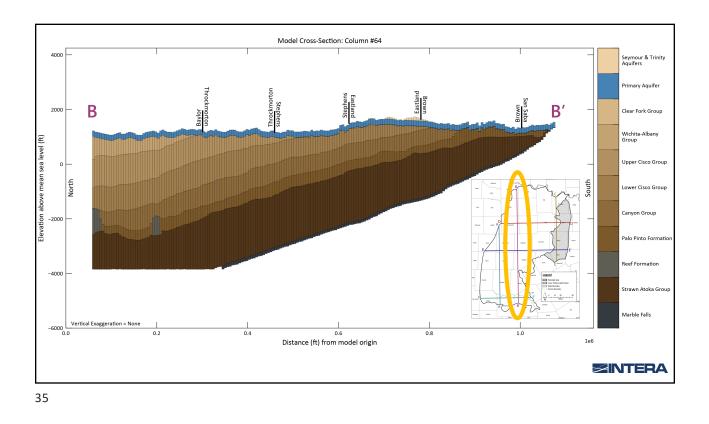


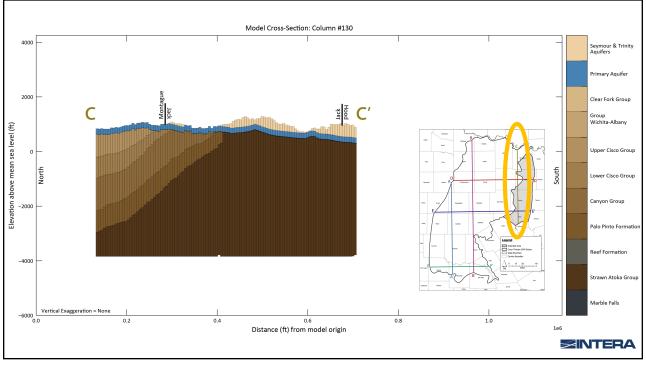


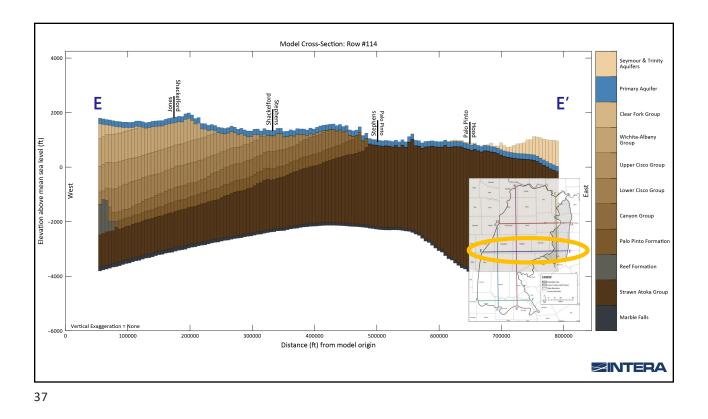




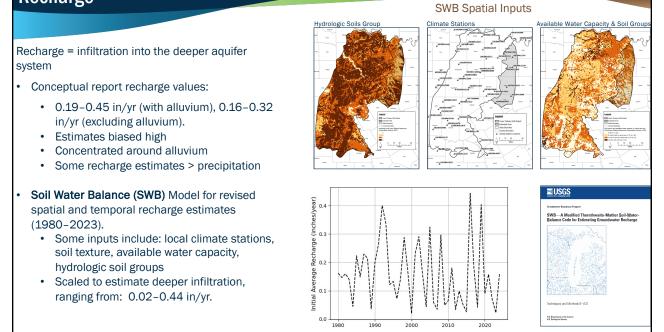




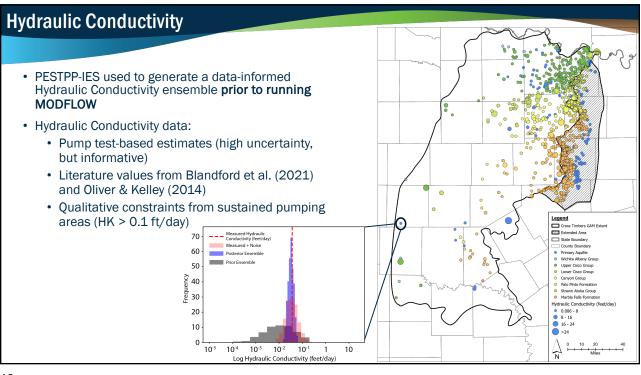




Recharge

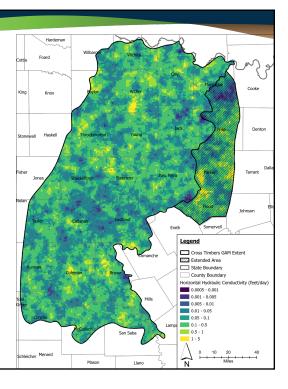


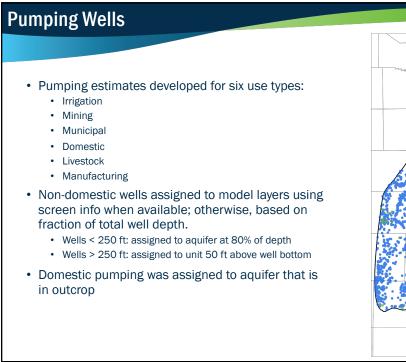


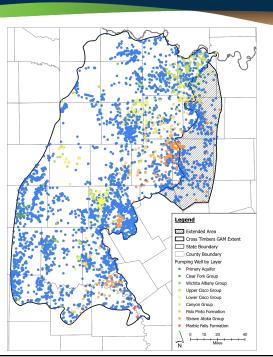


Hydraulic Conductivity

Final hyd	draulic	conduct	ivity dist	ribution	inform	ed by prie	or
ensemb	le, but	incorpor	ated gro	oundwate	er data	as well	
		<i>c</i> , , , ,		05.1			
Laura	A	Standard	M:	25th Demoentile	M	75th Demosratile	M
Layer Sevmour and	Average	Deviation	MINIMUM	Percentile	Median	Percentile	Maximi
Trinity Aquifers	8.6E+00	2.5E+00	1.9E-01	8.0E+00	1.0E+01	1.0E+01	1.0E+0
Primary Aquifer	1.9E-01	2.2E-01	4.9E-04	4.7E-02	1.1E-01	2.4E-01	2.0E+0
Clear Fork Group	4.9E-01	3.9E-02	9.1E-02	5.0E-01	5.0E-01	5.0E-01	5.0E-0
Wichita Albany							
Group	3.4E-01	1.7E-01	3.6E-03	1.8E-01	4.2E-01	5.0E-01	5.0E-0
Upper Cisco	3.75.01	1.9E-01	4.7E-04	8.6E-02	2.3E-01	5.0E-01	5.0E-0
Group Lower Cisco	2.7E-01	1.9E-01	4./E-04	8.6E-02	2.3E-01	5.0E-01	5.0E-0
Group	4.2E-01	1.5E-01	2.1E-03	3.8E-01	5.0E-01	5.0E-01	5.0E-0
Canyon Group	2.5E-01	1.9E-01	6.1E-04	7.7E-02	2.1E-01	5.0E-01	5.0E-0
Palo Pinto							
Formation	2.7E-01	2.0E-01	3.9E-04	7.5E-02	2.6E-01	5.0E-01	5.0E-0
Reef Formation	4.9E-01	3.8E-02	1.3E-01	5.0E-01	5.0E-01	5.0E-01	5.0E-0
Strawn Atoka							
Group	2.9E-01	1.9E-01	6.4E-04	1.1E-01	2.8E-01	5.0E-01	5.0E-0
Marble Falls Formation	4.3E-01	1.4E-01	2.8E-03	4.8E-01	5.0E-01	5.0E-01	5.0E-0

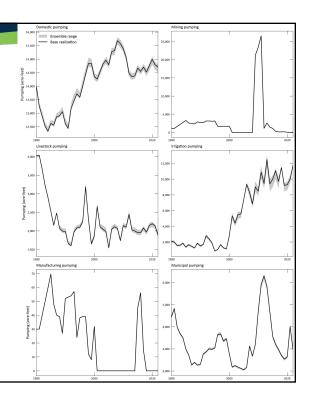


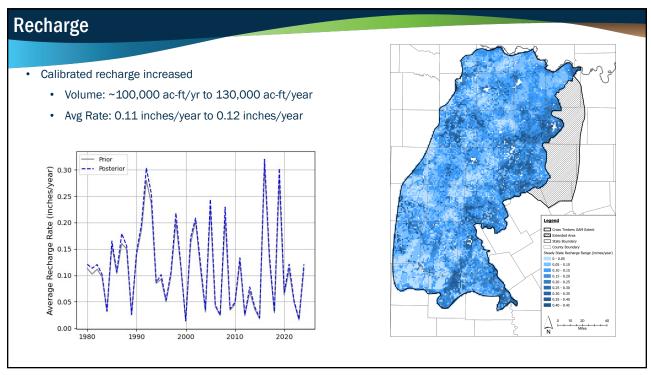




Pumping Rates

- TWDB data (1980–2022) used for municipal, industrial, mining, manufactoring, irrigation, and livestock pumping (1980–1984 interpolated).
- Domestic pumping rates based off population distributions and an assumed per capita rate of 100 gpd/person
- Pumping allocated to wells by use type, scaled by reported or estimated well yields.
- Calibration incorporates spatial uncertainty in well-based pumping rates.

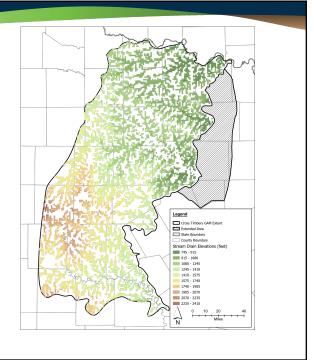




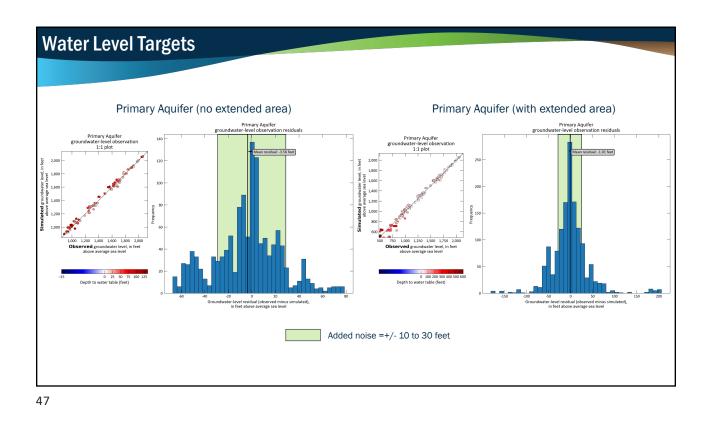
Stream Drains



- Intermittent and ephemeral streams
- Groundwater discharge
- Ensure topographic nature of groundwater table
- On average streamflow discharge increased during calibration by ~15,000 ac-ft/year

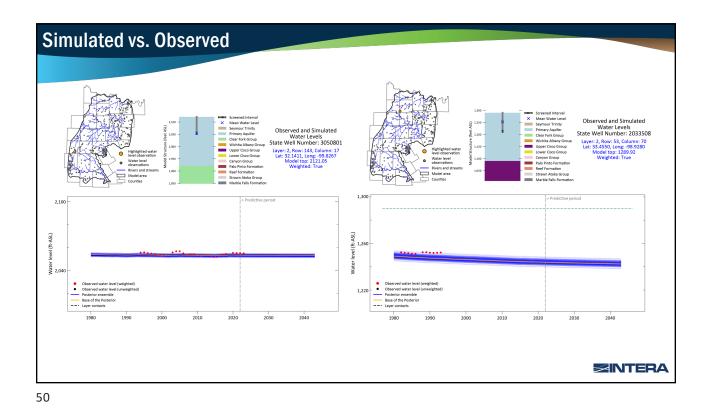


Water Lever largets	
 Water Level Targets Water level data obtained from TWDB and USGS 368 wells used as water level observations for the transient model calibration, 108 for steady state calibration Water level records varied in quality, longer record and higher frequency wells were weighted higher 	Image: Construction of the second of the



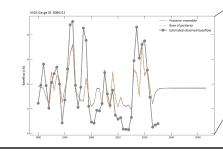
ater Lo	evel Tar	gets	\$						
	Hydrogeologic Unit	Count	Average Residual (feet)	Median Residual (feet)	Root Mean Square Error (feet)	Mean Absolute Error (feet)	Measured Range (feet)	<u>RMSE</u> Range (<10%)	
Over Official Aquifer Boundary	Seymour & Trinity Aquifers	650	-6.4	-1.6	33.4	25.9	783.1	4.3%	
Over (Aqu Bour	Primary Aquifer	1276	19.8	18.5	50.7	39.2	1330.1	3.8%	
Over Entire Model Study Area	Primary Aquifer	1433	17.4	17.5	59.7	44.7	1834.3	3.3%	The second secon

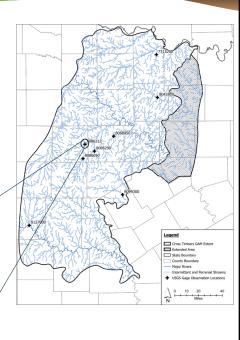
Water Level Targets

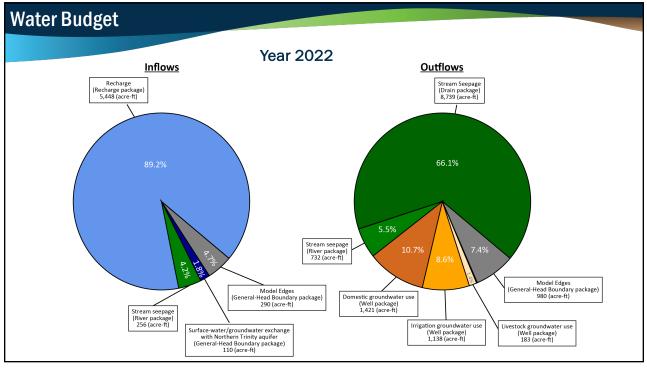


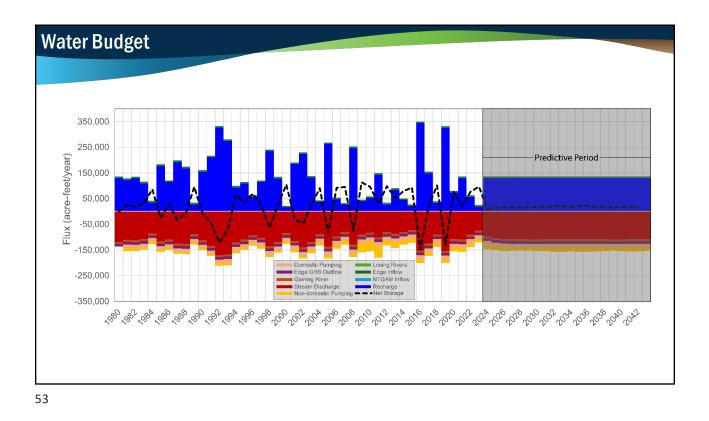


- Statistical comparison with conceptual report (Table 4-10 vs. CR Table 4-8):
 - Average and median values in good agreement
 - · Min and max values differ due to model smoothing effects
- Despite low weighting, the model captures general trends in groundwater discharge to streams.







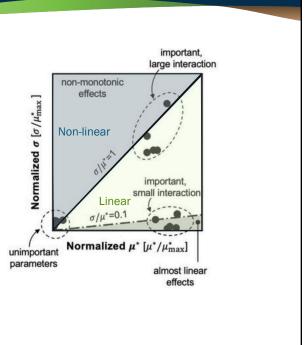


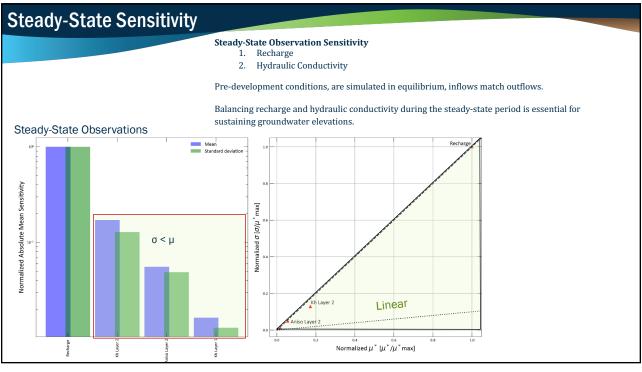


Model Sensitivity

- Method of Morris (Morris, 1991) for Global Sensitivity Analysis
 - Overall model sensitivity
 - Sensitivity by observation group
- Each parameter sampled four times within its posterior distribution

Parameter	Туре	Layer(s)	Runs
Horizontal Hydraulic Conductivity	constant	1, 3-11	40
Horizontal Hydraulic Conductivity	zone	2	4
Vertical Hydraulic Conductivity	constant	3-11	36
Vertical Hydraulic Conductivity	zone	2	4
Specific Storage	constant	2-11	40
Specific Yield	constant	1	4
Specific Yield	zone	2	4
Recharge Rates	constant	1-2	4
River Conductance	constant	1-2	4
Stream Drain Conductance	constant	1-2	4
Drain Edge Conductance	constant	3-11	4
Domestic Pumping Rates	constant	1-2	4
Municipal Pumping Rates	constant	1-2	4
Livestock Pumping Rates	constant	1-2	4
Irrigation Pumping Rates	constant	1-2	4
Total Run	5		164





Overall Model Sensitivity

High Frequency Groundwater Elevation Sensitivity

- 1. Recharge
 - 2. Horizontal Hydraulic Conductivity
- 3. Specific Yield

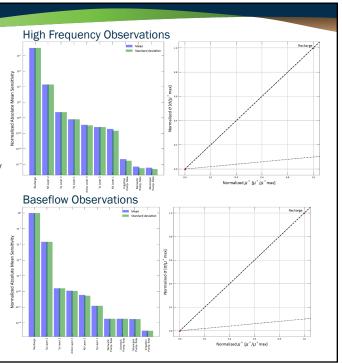
"The sensitivity of groundwater levels throughout the primary aquifer to recharge and horizontal hydraulic conductivity is expected, as the balance of the two correlated parameters directly controls simulated groundwater levels."

Baseflow Observation Sensitivity

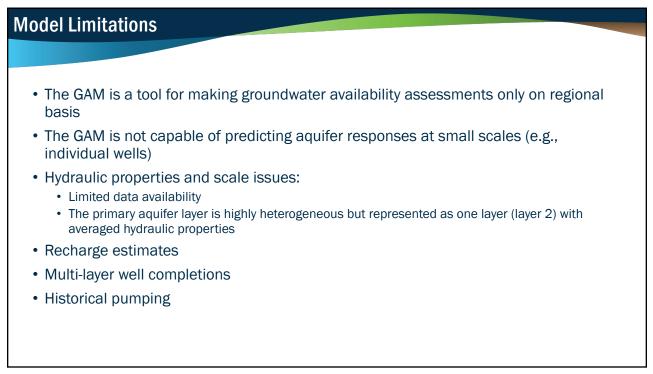
- 1. Recharge
- 2. Specific Yield
- 3. Specific Storage

"Recharge is the main inflow component, directly influences the total discharge volume."

"Lower storage values lead to flashy baseflow responses to recharge fluctuations. In contrast, higher storage values support more sustained baseflows during dry periods."





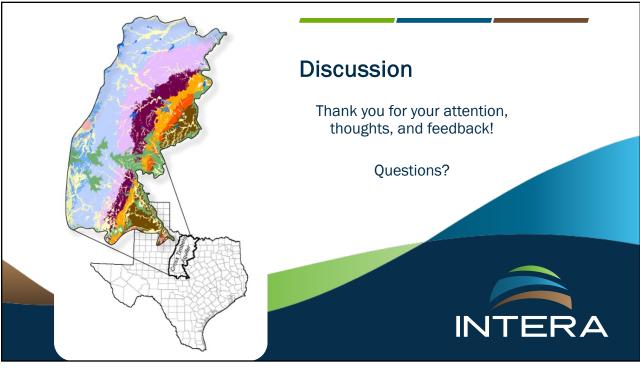




Final Thoughts
Well calibrated model, despite data limitations
 Aligns with conceptual understanding, while also providing more spatial and temporal understanding
 Scripted workflow, dynamic tool, easily updated with new data/conceptual understanding
 Robust uncertainty analysis will provide better predictive capabilities and additional confidence in management decisions.
60



Contact informationStephanie Moore, P.G. (INTERA)505-235-9561SMoore@intera.comDaryn Hardwick, Ph.D. (TWDB)512-475-0470Daryn.Hardwick@twdb.texas.govWeb information:https://www.twdb.texas.gov/groundwater/models/gam/cstb/cstb.asp



Attachment 3. Summary of Questions and Answers

1. Roberto Anaya asked: Why was a Texas State Plane Coordinate System (a Lambert Conic Conformal projection optimized for most accurate shapes and directions) used instead of the GAM coordinate system (an Albers Equal Area projection used to optimize area)? Our TWDB calculations rely on most accurate area such as acre-foot units.

Response: At the time this project began, the GAM coordinate system had not yet been established with the European Petroleum Survey Group (EPSG) code by TWDB. EPSG codes provide a standardized, easy-to-reference system for specifying coordinate reference systems, ensuring consistent and accurate mapping across different software and datasets, and are especially useful in coding contexts where quick, unambiguous spatial references are needed. An EPSG code for the GAM coordinate system was not developed until the Cross Timbers numerical model development was well under way.

Within the living, scripted workflow, there is a function that will change the coordinate system of anyone of the datasets on the fly.

2. Michaela Pedrazas asked: Regarding the water level targets, 1) When averaging water levels to get annual values, did you filter water levels to just winter water levels to avoid including the effect of pumping? 2) What are you hanging the water levels from? (10m DEM?)

Response: For averaging annual water levels, we used a rolling average technique with the goal of smoothing out any impacts from pumping. We have an appendix in the report with all the hydrographs of raw data. Most of our water levels are actually collected during winter months so we had minimized any bias from pumping.

Yes, water levels are hung from the 10-m DEM. Often, elevation data provided by drillers is inaccurate (often ready by handheld GPS units), so we re-sampled our well locations to the DEM, which has a 30-foot by 30-foot resolution.

3. Neil Blandford had comment: The way we had done the conceptual model, is that the recharge can exceed precipitation at a given location if it's focused recharge, where runoff is focused to a particular location. It can and often does exceed the precipitation at that location.

Response: Yes, we understand that recharge has very high level of uncertainty because of lack of data. There is a large amount of variability in diffuse and focused recharge and relatively little data, particularly for the Cross Timbers study area. Better data for recharge is one of the areas that we specifically call out as having room for future improvement.

A good amount of focused recharge spots ended up aligning with our rivers and drain cells. The river package specifically would still allow focused recharge to happen (where the river is losing water) in quantities greater than precipitation.

4. Neil Blandford asked: Have you done any type of sensitivity on the sharp interface boundary which is essentially a hydraulic boundary of sorts, which I think would lie pretty much at the



bottom of your layer 2? And the way I understand the system, you're recharge and pretty much all the pumping base flow, et cetera is really happening in that layer 2. And I'm wondering if you've done any type of sensitivity on that, which would, you know, basically be cutting off all of the model below layer 2?

Response: Yes, we have done sensitivity analysis and overall sensitivity is minimal. Additional details are available in the model report. We have drain edge parameters at the edge of the model and at the bottom of layer 2 (the primary aquifer). We used those to represent the interface at the bottom to see if we had heads in deeper layers that were building up too much, essentially allowing water into the primary aquifer (layer 2) and pushing that interface up or down. The overall sensitivity of those edge drains was minimal.

Additionally, we did particle tracking in deeper layers just to see that those particles remained in the deeper layers. We wanted to be sure that we didn't see a particle go from one of those deep layers up into the shallow flow system over the simulation period of 60 years.

One of the major challenges of this model is knowing where that interface sits because we do not have much spatial coverage and data to show where the fresh-saline interface is located. As you showed in the conceptual model, there are some locations where it may be as deep as 500 feet, but overall, it is closer to 200 feet. Additional data regarding the fresh-saline interface is big area for future model improvements.

